

# **Validation of FDS Predictions on Fire-Induced Flow: A Follow-up to Previous Study**

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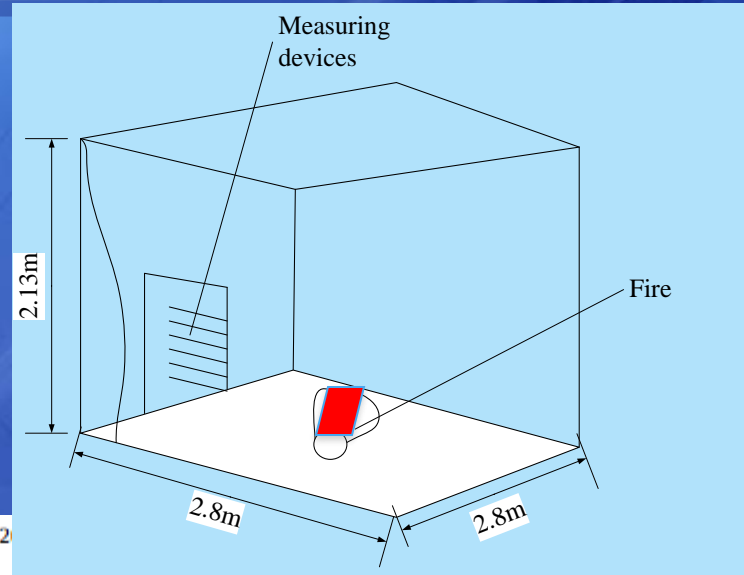
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# Motivation

- ❖ In an earlier study, Steckler's experiments were modeled using FDS, a zone model & correlation



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## An analysis of compartment fire doorway flows

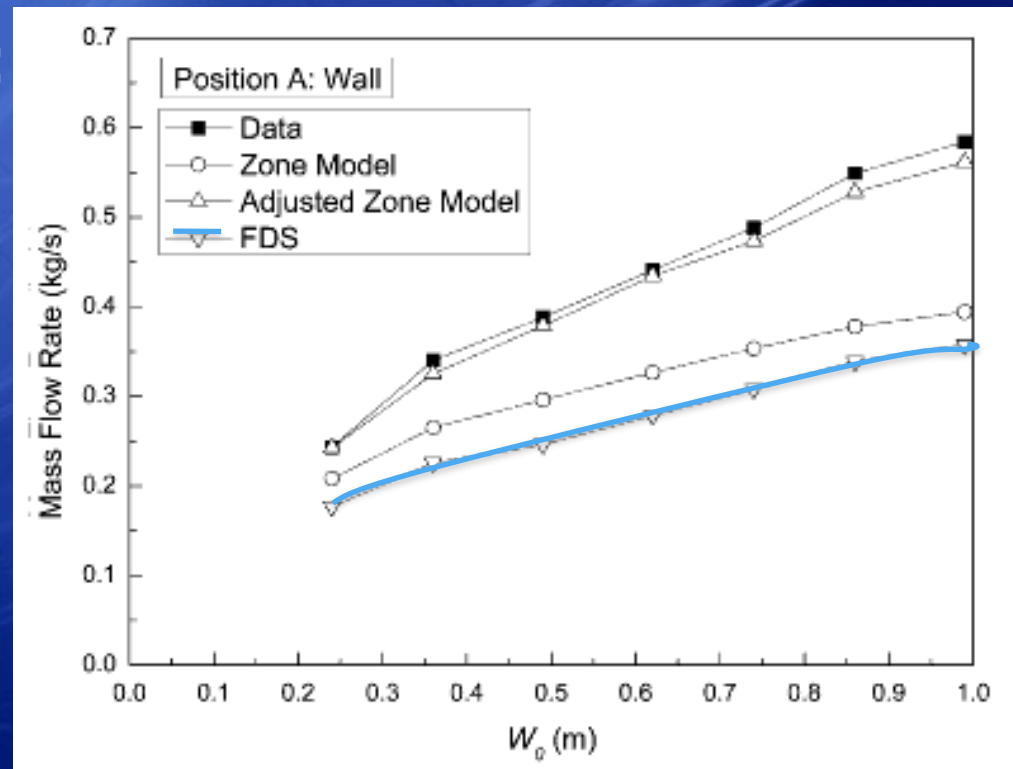
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# Motivation

- ❖ It was found that the FDS model lacked the ability to accurately predict the flow rate
- ❖ & and other aspects:
  - Neutral plane
  - Layer height
  - Lower Temperature.
- ❖ 50 % discrepancy in flow.
- ❖ The current work attempts to improve the FDS results.



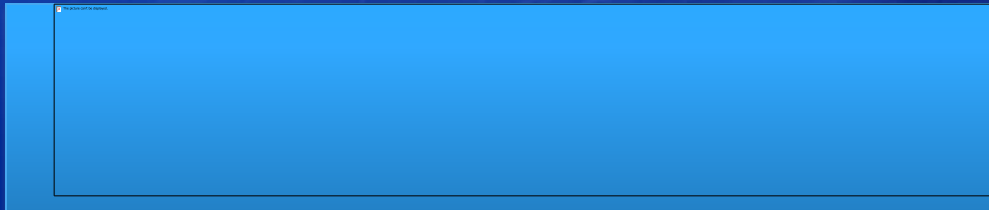
# Motivation

## ❖ Previous FDS

- FDS v5.1.0
- 5 cells across the face of the 30 cm burner
- Vent boundary condition
  - Outflow dynamic pressure = 0
  - But from Bernoulli:

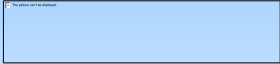
## ❖ New FDS

- A little finer grid
- Boundary extended beyond the vent
- Adjustment for burner shape against wall
  - Square vs round

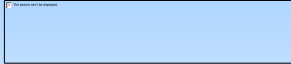


# Approach

**Finer resolution**


$$D^* / \delta x = 5.3$$




$$D^* / \delta x = 6.3$$

# Approach

- ❖ The **same** grid size (uniform 5 cm) is used in the **FDS validation** by NIST for the prediction of the hot gas layer temperature and velocity profile at the doorway based on the same Steckler's experiments.
- ❖ An additional simulation with a smaller grid of 2.5 cm revealed that the difference between the results for the two grid sizes is negligible. Thus, the grid size of 5 cm is regarded as **grid independent**.

# Approach

## Radiative fraction

Default **0.35**  
for LES in  
FDS

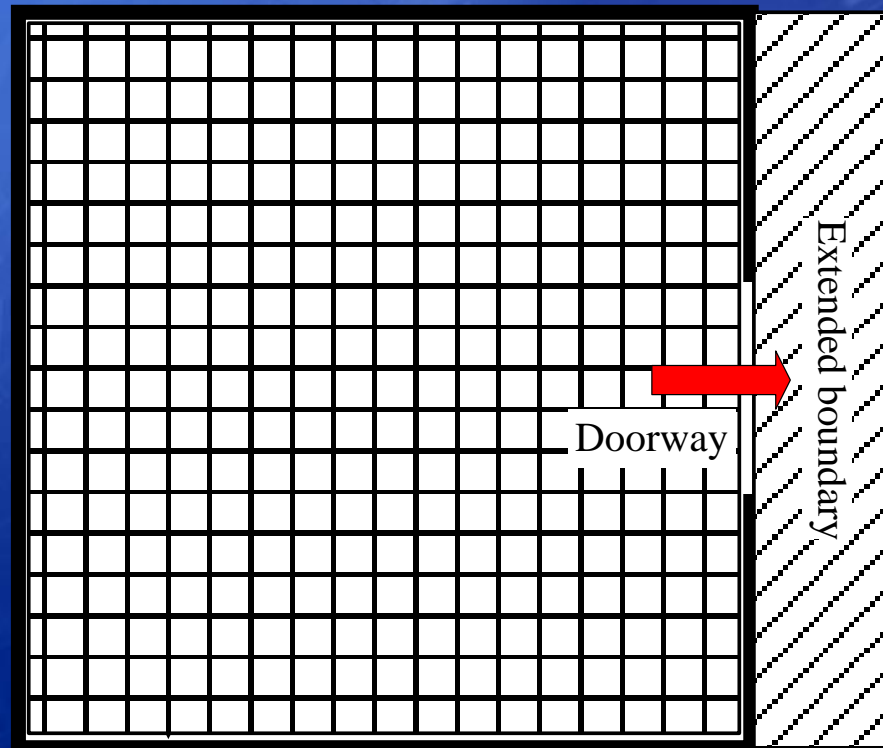
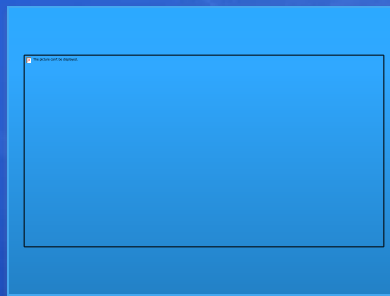


Updated **0.14**  
based on  
Tewarson's  
data for  
methane



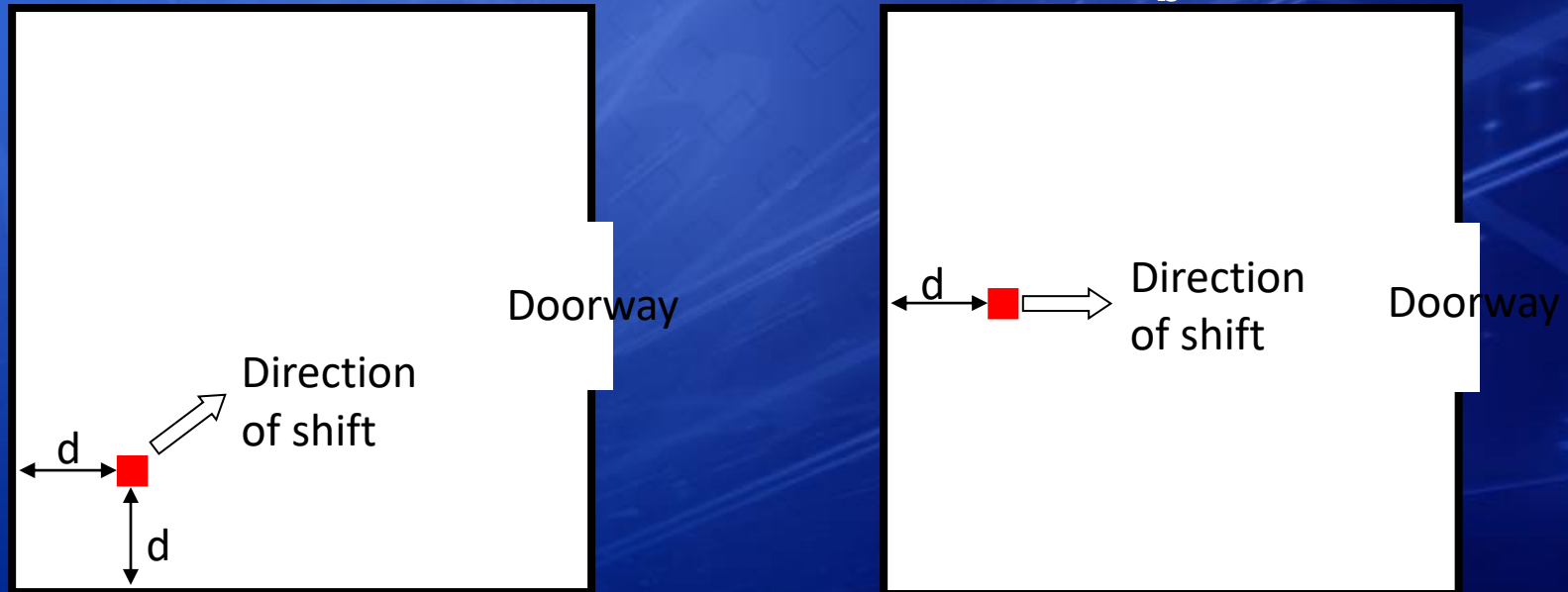
# Approach

- ❖ An **extension** of computational domain.
- ❖ The distance that the domain was increased was scaled to the effective diameter,  $D_d$  of the doorway. **Used  $0.5 D_d$**  (to get flow rate to 5%)



# Approach

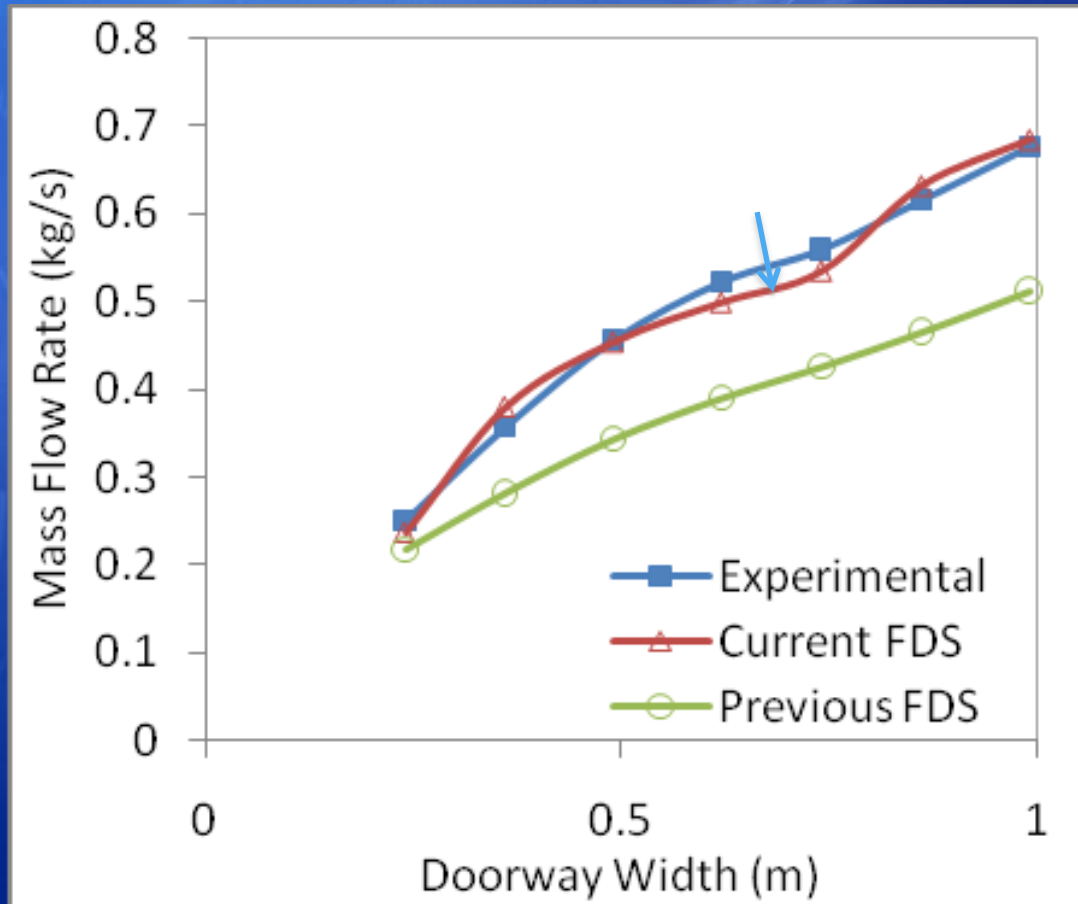
- ❖ A **shift** of fire location to account for the lost entrainment by the square fire used in FDS. The distance is also scaled to the **burner diameter,  $D_b$** , in an attempt to investigate possible correlations. **Used  $d \sim 2D_b$**



Shift of fire locations for position B (corner) and C (against wall).

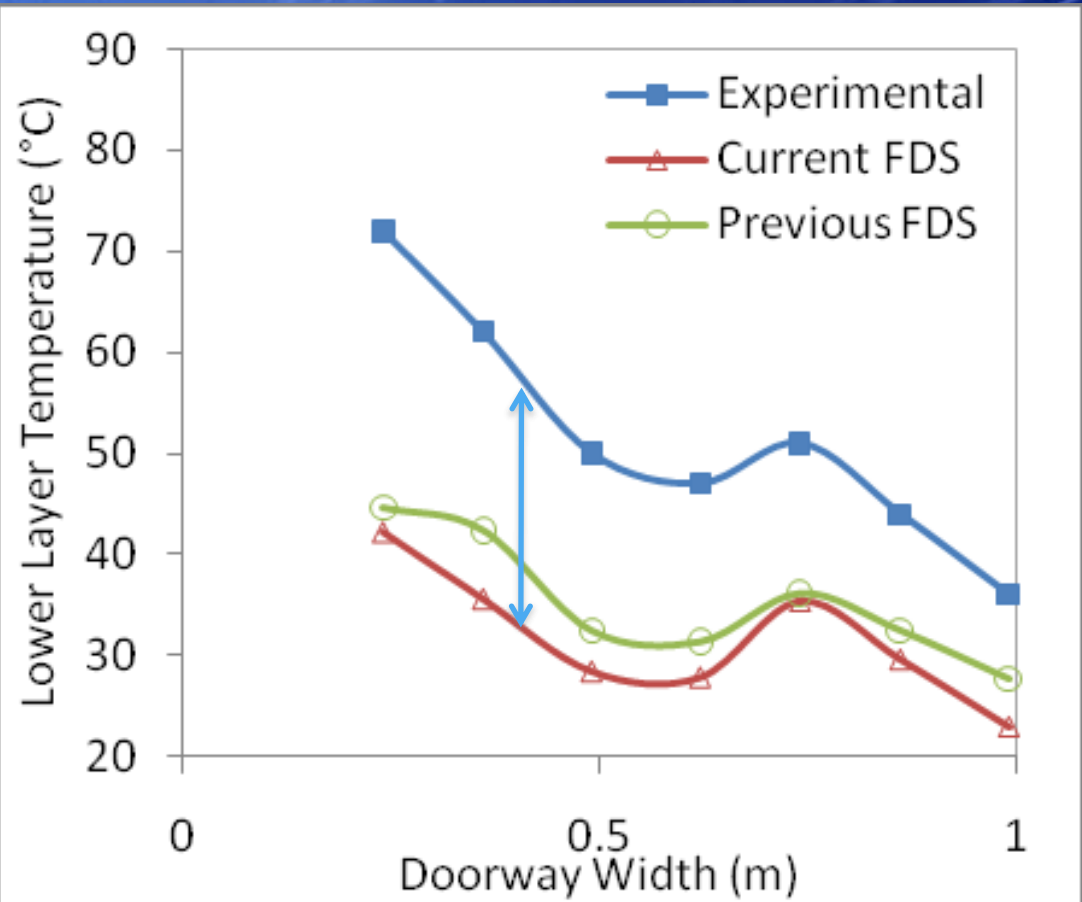
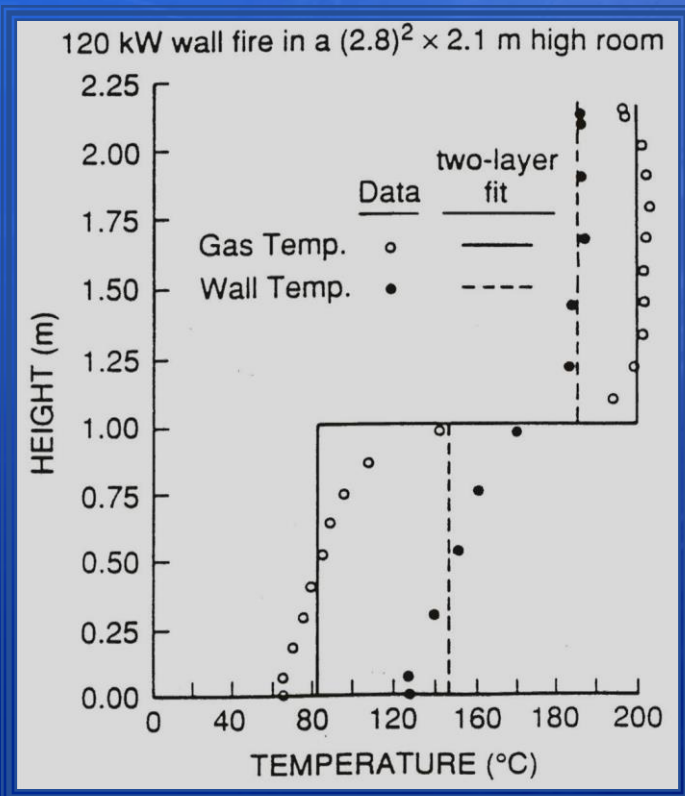
# Results

- ❖ Fire Source at Center (Position A) : Mass flow rate



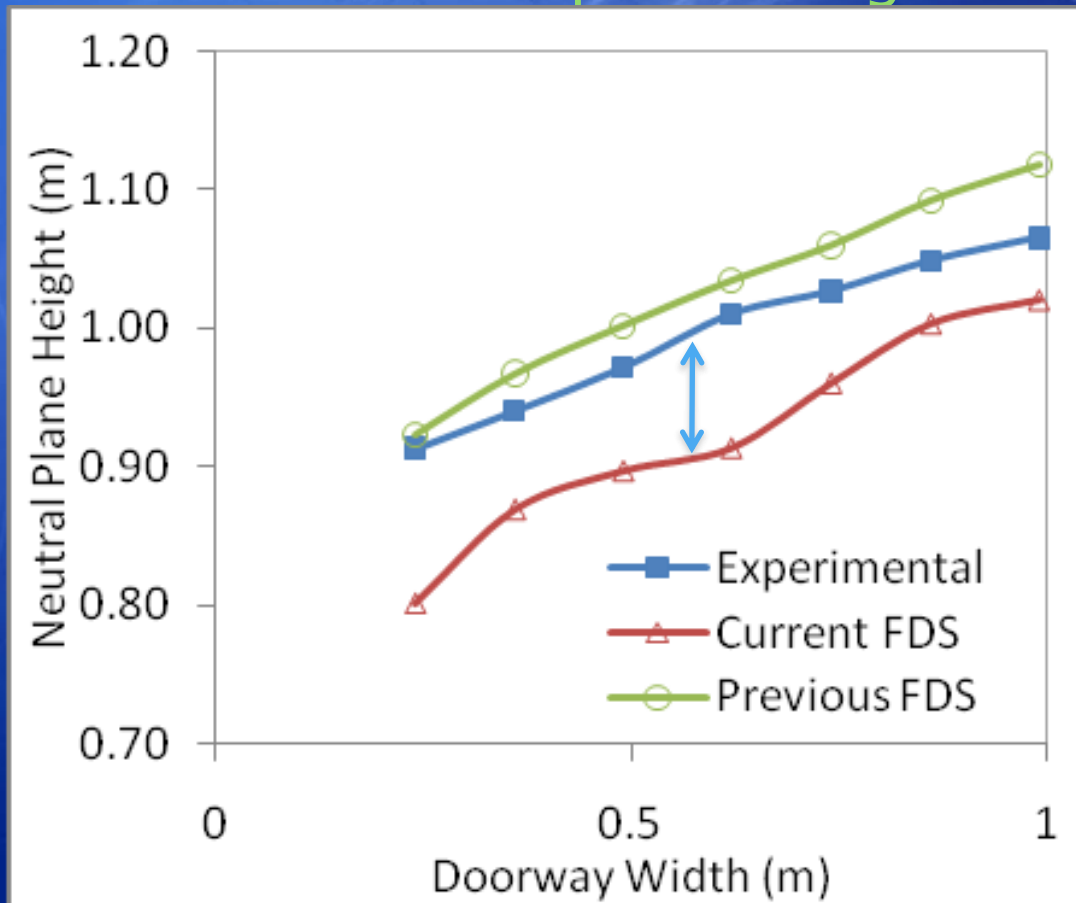
# Results

- ❖ Fire Source at Center (Position A):
  - ❖ Lower layer temperature



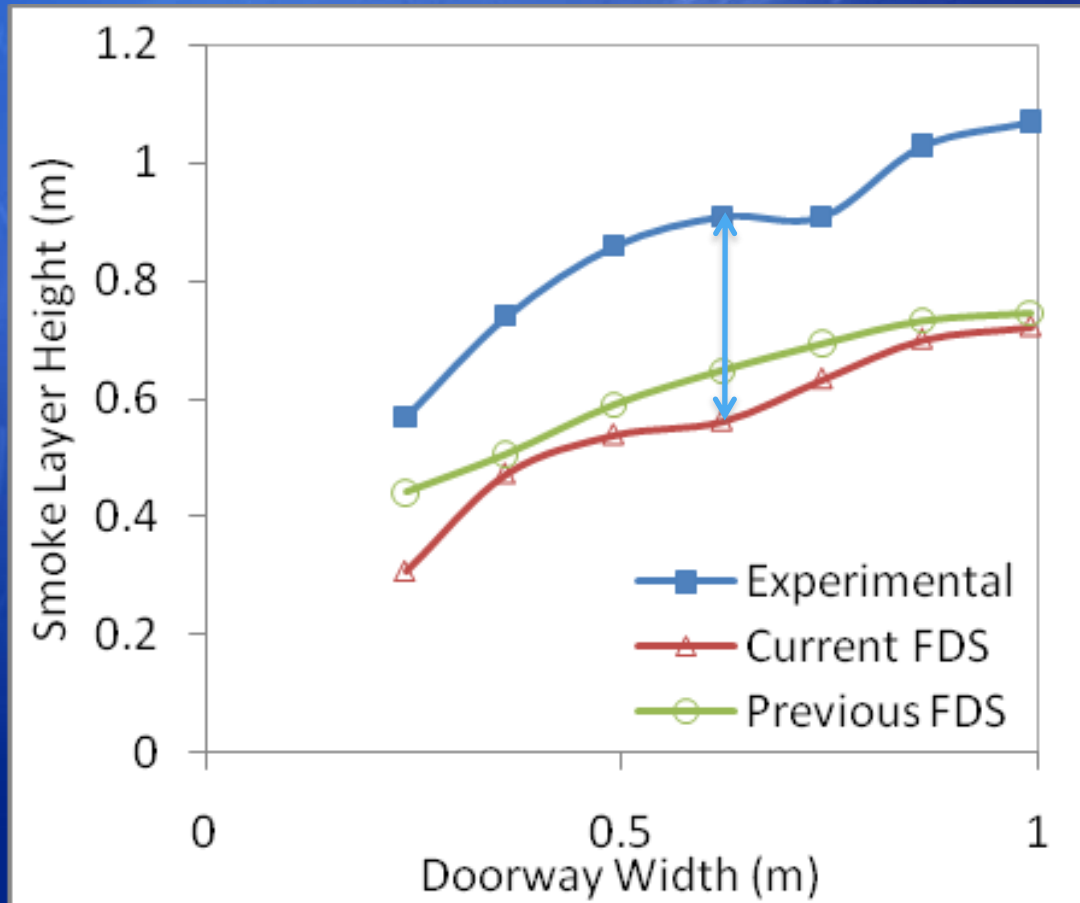
# Validations

- ❖ Fire Source at Center (Position A) :
  - ❖ Neutral plane height



# Validations

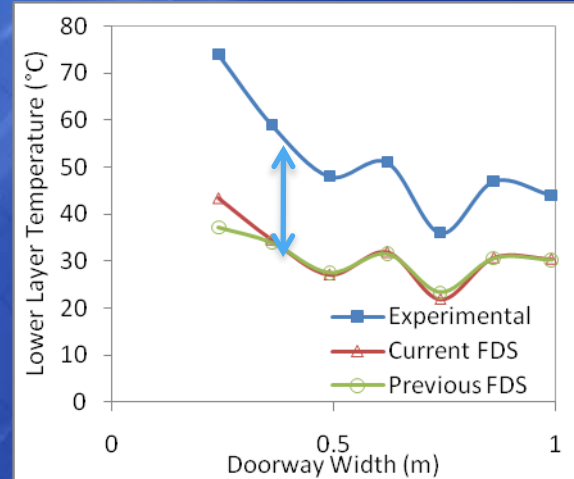
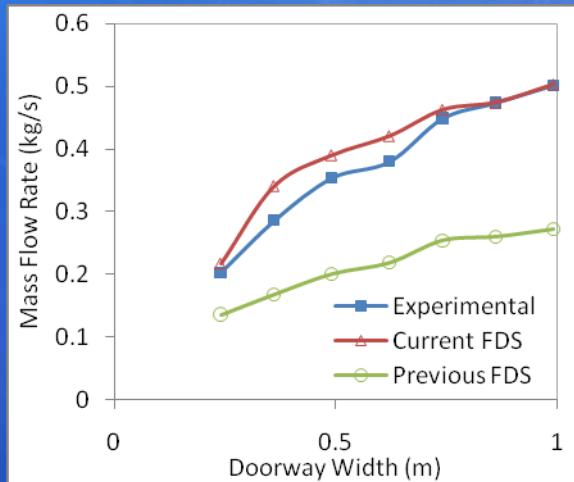
- ❖ Fire Source at Center (Position A) :
  - ❖ Smoke layer height



# Results and Discussions

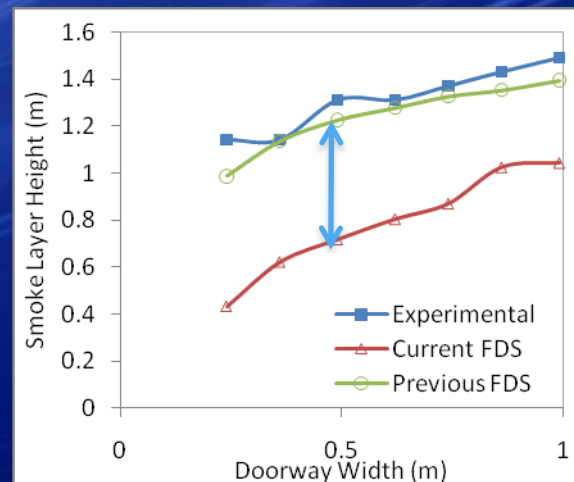
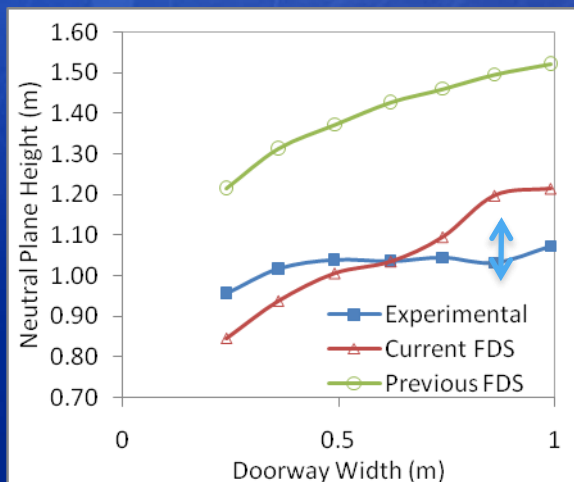
## ❖ Fire Source at Corner (Position B)

Flow Rate



Lower Temp

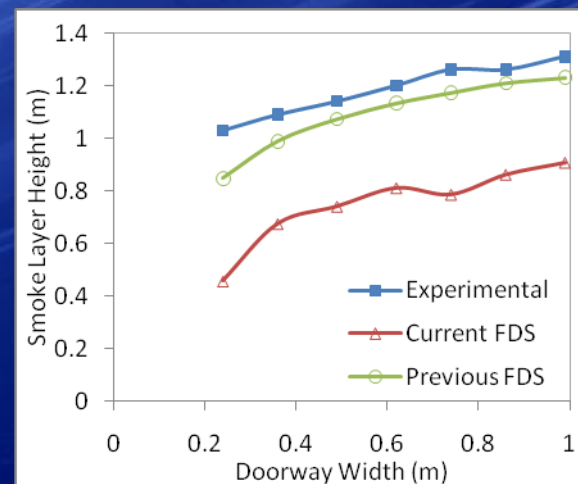
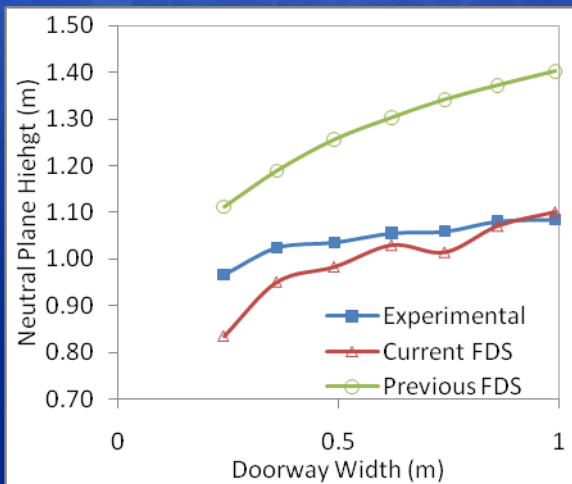
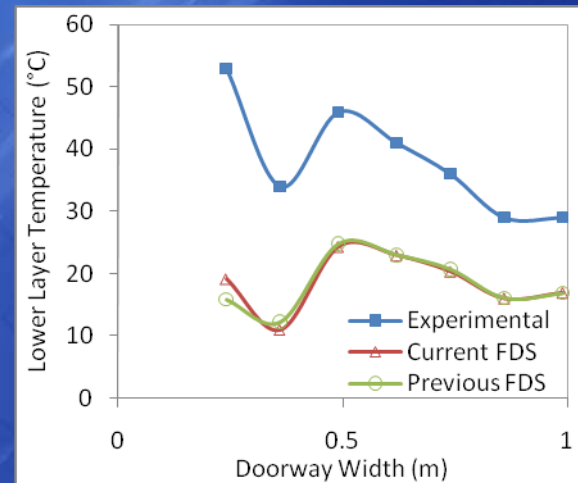
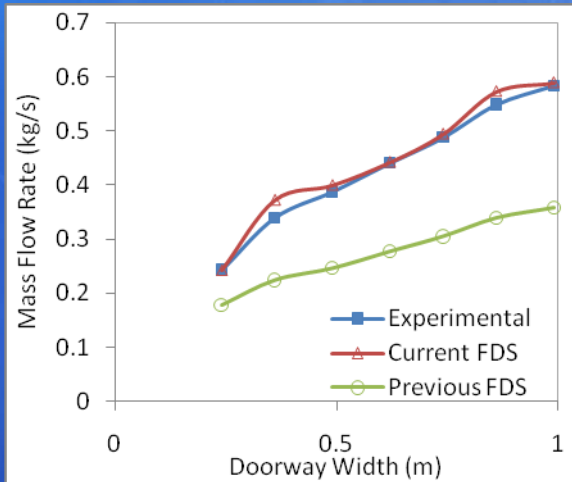
Neutral



Layer

# Validations

## ❖ Fire Source at Wall (Position C)





# Discussion

1

The improvements on model inputs made to the FDS simulation allowed significant improvements to the prediction of mass flow rates for all three positions of the fire source.

2

There is not much improvement for the remaining three parameters being compared: neutral plane height, low layer temperature and smoke layer temperature.

3

Since these three zone-model based parameters are calculated by an integral approximation. It is not advised that they are predicted by using FDS.

mass flow rate ~ 5 %, Neutral plane +/- 10 %,  
Layer & Lower  $T$  - 40 %,

# Discussion

## Two rules of thumb

A distance of  $0.5D_d$  (effective diameter of doorway) from the vent on the computational domain is needed to avoid the possible inaccurate boundary conditions (within 5%).

For fire located at the corner and against the wall, a shifted distance for the burner of  $2D_b$  (diameter of burner) is needed to compensate the entrainment loss (within 5%).

**Thank You !**