## ACCEPTANCE CRITERIA IN FIRE SAFETY ENGINEERING: A REVIEW AND CASE STUDY Daniel Rosberg

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# Introduction

- Methods to verify safe egress
  - Qualitative methods
  - Scenario-based methods
  - Risk-based methods
- Scenario-based methods
  - ASET/RSET-analysis
  - Fractional effective dose (FED) concept

- Traditional ASET/RSET analysis
  - Simple (yet complex)
  - Fire model to find ASET
    - evaluated against **absolute values**
  - Evacuation software to find RSET
- Fractional effective dose (FED) concept
  - More common when evacuation through smoke
  - More complex method
  - Fire model (CFD) to calculate concentrations
  - Evacuation model to calculate dose

# **Acceptance criteria for absolute values**

- Defined in some building regulations
  - Sweden
  - New Zealand
- European initiative
  - Still variation between countries
- No uniform set of criteria in a global perspective



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| Criteria                         | Swedish building regulations <sup>(1)</sup><br>BBRAD 3  | New Zealand Building Code <sup>(1)</sup><br>C/VM2               |
|----------------------------------|---|---|
| Smoke layer above<br>floor level | Smoke layer ><br>1.6 + (ceiling height)*0.1 [m]   | -   |
| Visibility                       | Visibility > 10 m (spaces > 100 m²)   | Visibility <sup>(2)</sup> > 10 m (spaces > 100 m <sup>2</sup> ) |
| Visibility                       | Visibility > 5 m (spaces < 100 m <sup>2</sup> or<br>spaces where queuing start early<br>in the evacuation)  | Visibility <sup>(2)</sup> > 5 m (spaces < 100 m <sup>2</sup> )  |
| Thermal radiation                | Radiation < 2.5 kW/m <sup>2</sup> or a short-<br>term radiation of < 10 kW/m <sup>2</sup><br>combined with a maximum<br>energy dose of < 60 kJ/m <sup>2</sup> in<br>excess of the energy from a<br>radiation level of 1 kW/m <sup>2</sup> | Requirements for radiation<br>exposure along egress routes.     |
| Temperature                      | Temperature < 80 °C   | FED <sub>thermal</sub> criteria specified                       |
| Carbon monoxide<br>toxicity      | [CO] < 2000 ppm   | FED <sub>co</sub> criteria specified                            |
| Carbon Dioxide<br>toxicity       | [CO <sub>2</sub> ] < 5%   | -   |
| Oxygen availability              | [O <sub>2</sub> ] > 15%   | -   |
| FED                              | -   | $FED_{CO} < 0.3$ $FED_{thermal} < 0.3^{(2)}$                    |

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# **Acceptance criteria for absolute values**

- Simple to work with
- Low sensitivity to changes in the combustibles
- Generally well accepted

- Required inputs
  - Fire size,
  - Growth rate,
  - CO yield,
  - $-CO_2$  yield,
  - Soot yield
  - Heat of combustion

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# FED tenability acceptance criteria

- Some design situations require alternative measures to assess the consequences of a certain fire scenario
  - When exposed to smoke during longer durations
  - Road tunnels
  - Rail tunnels
  - Sprinklered buildings
- It is common that the responsibility lies with the designer to asses:
  - the methodology to use
  - Which asphyxiant (and/or irritant) gases to consider
  - acceptable accumulated dose to verify life safety against

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# **FED tenability acceptance criteria**

- Common values
  - FED<1.0
    - 50 % of the population being susceptible
  - FED<0.3
    - 11 % of the population being susceptible

- Input yield data
  - highly dependent on fire conditions
  - Difficult to find reliable information (seldom reported)

# **Purpose and goals**

"Investigate the consequences of applying different methods and acceptance criteria to verify fire life safety." Goals:

- 1. How the fire safety outcome is affected by the method used (i.e. absolute values or FED).
- 2. How the fire safety outcome is affected by the acceptance criteria (e.g. different acceptance criteria for the same variable)
- 3. Address the challenges an engineer faces when working with alternative methods and acceptance criteria compared to traditional or regulated approaches.

# **Case study: Geometry**

# Simple geometry

- IMO test 10
- Cabin arrangement on a passenger ship
- 12 cabins
- People asleep
  - No movement
  - 23 occupants



# **Case study: Geometry**

- FDS 6.7.0
- Grid size 5 to 10 cm
- Room height 2.8 m
- Openings at exits
  - Door width x 0.6 m
- Fire source in Cabin #9
- Data recorded at 2 m height



| Yield                                      | Units | BBRAD 3 | NIST sofa <sup>‡</sup> |
|--|-------|---------|------------------------|
| Peak fire size (no sprinklers)             | MW    | 5       | _*                     |
| Growth rate (t-squared)                    | kW/m² | 0.047   | _*                     |
| Heat of combustion                         | MJ/kg | 20      | _*                     |
| Fraction of Hydrogen in soot               | -     | O.1†    | 0.1 <sup>†</sup>       |
| Yields (per gram of fuel consumed)         |       |         |                        |
| Soot                                       | [g/g] | O.1     | _*                     |
| Carbon Dioxide (CO <sub>2</sub> )          | [g/g] | 2.5     | 1.59                   |
| Carbon Monoxide (CO)                       | [g/g] | 0.1     | 0.0144                 |
| Hydrogen Cyanide (HCN)                     | [g/g] | -       | 0.0035                 |
| Hydrogen Chloride (HCl)                    | [g/g] | -       | 0.018                  |
| Nitrogen Dioxide (NO <sub>2</sub> )        | [g/g] | -       | 0.07                   |
| Acrolein (C <sub>3</sub> H <sub>4</sub> O) | [g/g] | -       | 0.008                  |
| Formaldehyde (CH <sub>2</sub> O)           | [g/g] | -       | 0.02                   |

At a glance

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# **Methodology: Two cases**

### BBRAD 3 case

- Well defined input data and acceptance criteria
- CO, CO<sub>2</sub> and soot

#### - Simple chemistry

- Single mixing-controlled reaction
- Fuel molecule contains only C, O, H, and N.
- $-\,C_{4.56}H_{6.56}O_{2.34}N_{0.4}$

# NIST Sofa case

 HCN, HCl, NO<sub>2</sub>, C<sub>3</sub>H<sub>4</sub>O and CH<sub>2</sub>O also considered

#### - Complex chemistry

- Additional species were lumped in the model
- The volume fractions calculated from the stoichiometric coefficients of the primitive species

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## **Results: BBRAD 3 case**

- + BBRAD Criteria 1 Layer > 1.6 + 0.1\*ceiling height [m]
- $\times$  BBRAD Criteria 2a Visibility > 10 m in rooms > 100 m<sup>2</sup>
- BBRAD Criteria 2b Visibility > 5 m in rooms < 100  $m^2$
- □ BBRAD Criteria 3 Radiation < 2.5 kW/m<sup>2</sup>
- ♦ BBRAD Criteria 4 Temperature < 80 °C
- ♦ BBRAD Criteria 5a CO < 2000 ppm

- $\times$  BBRAD Criteria 5b CO<sub>2</sub> < 5%
- BBRAD Criteria 5c  $O_2 > 15\%$
- $\triangle$  FED < 0.3
- $\triangle$  FED < 1.0
- △ FIC < 1.0



## **Results: NIST Sofa case**

- + BBRAD Criteria 1 Layer > 1.6 + 0.1\*ceiling height [m]
- $\times$  BBRAD Criteria 2a Visibility > 10 m in rooms > 100 m<sup>2</sup>
- BBRAD Criteria 2b Visibility > 5 m in rooms < 100 m<sup>2</sup>
- □ BBRAD Criteria 3 Radiation < 2.5 kW/m<sup>2</sup>
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- $\times$  BBRAD Criteria 5b CO<sub>2</sub> < 5%
- BBRAD Criteria 5c  $O_2 > 15\%$
- $\triangle$  FED < 0.3
- $\triangle$  FED < 1.0
- △ FIC < 1.0



#### At a glance

| + BBRAD Criteria 1 - Layer > 1.6 + 0.1*ceiling height [m]                    | $\times$ BBRAD Criteria 5b - CO $_2$ < 5% |
|--|---|
| $\times$ BBRAD Criteria 2a - Visibility > 10 m in rooms > 100 m <sup>2</sup> | BBRAD Criteria 5c - $O_2 > 15\%$          |
| BBRAD Criteria 2b - Visibility > 5 m in rooms < 100 m <sup>2</sup>           | $\triangle$ FED < 0.3                     |
| BBRAD Criteria 3 - Radiation < 2.5 kW/m <sup>2</sup>                         | ▲ FED < 1.0                               |
| ♦ BBRAD Criteria 4 - Temperature < 80 °C                                     | ▲ FIC < 1.0                               |

♦ BBRAD Criteria 5a - CO < 2000 ppm





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# Discussion: How the fire safety outcome is affected by the method used?

- Using FED as a criteria will allow for longer ASET compared to using absolute tenability criteria
  - Impaired visibility is the tenability criteria first exceeded
  - Takes 4-8 times longer for FED to exceed 0.3 (without additional species)
- As more species were added
  - FIC<1 matches the visibility criteria
  - Less difference between FED<0.3 and visibility
  - The "simple model" became a good indicator of ASET

# Discussion: How the fire safety outcome is affected by the acceptance criteria ?

- The tenability criteria for visibility (both 5 and 10 m) and layer height is exceeded roughly at the same time
  - Two-zone model?
  - Different layer height criteria would most likely have little influence on the results
- Difficult to estimate in the BBRAD case since FIC<1 and FED<1 were not exceeded</li>
- With additional species
  - FIC<1 was first exceeded</li>
  - FED<0.3 approx. one minute later
  - FED<1 approx. one minute after FED<0.3

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# **Discussion: The challenges an engineer face**

- Applying absolute tenability criteria to a case is pretty straight-forward
  - Mandated input data and acceptance criteria reduce the risk of not getting approval
- Using FED concepts is more difficult
  - No uniform agreement on acceptance criteria
  - No uniform agreement on which species to add
  - Difficult to find reliable data (a big part of this study)
  - Complex chemistry might introduce a greater risk of user-error
- The tools (FDS) can handle the complexity
- Evacuation models need to account for reduced walking speed in smoke

# Thank you!

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