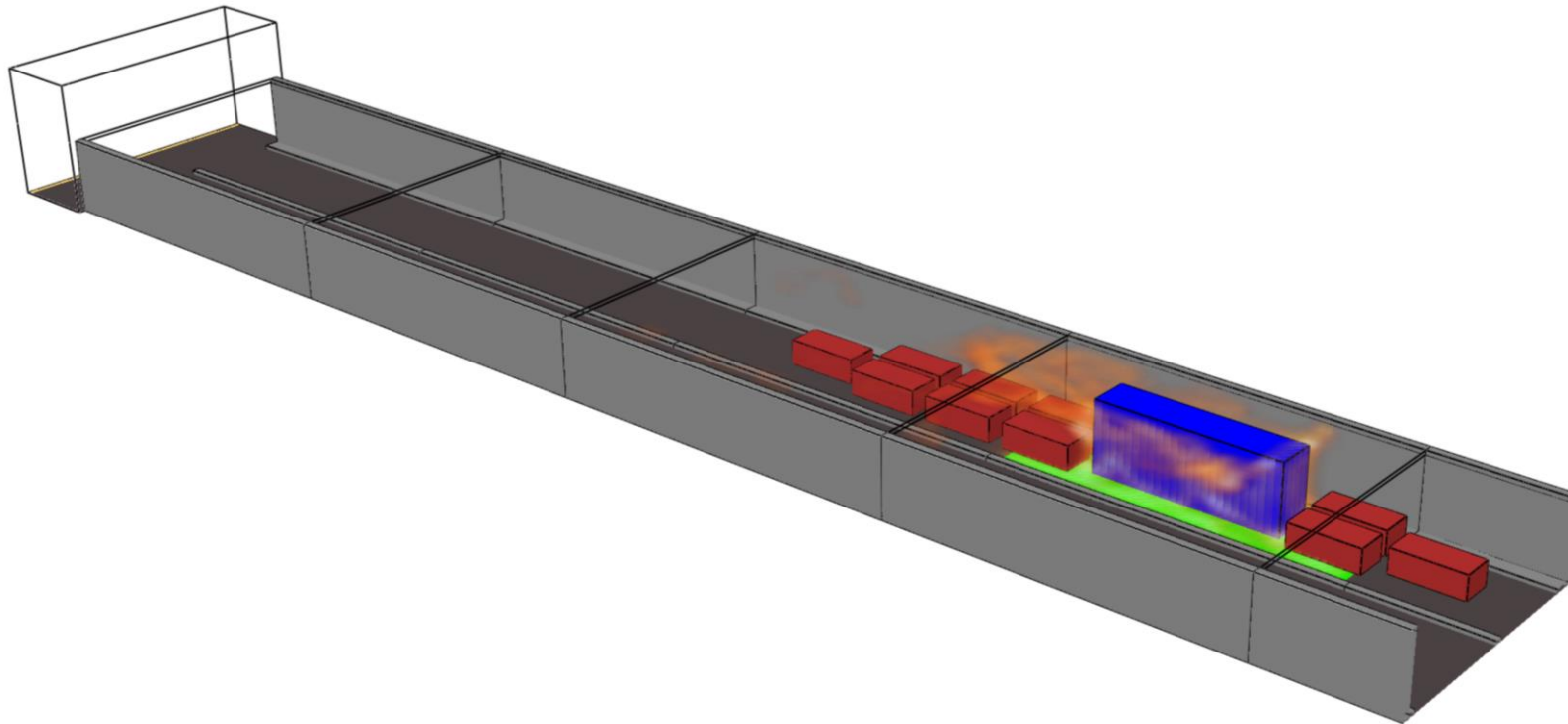


# Structural fire assessment of an existing tunnel

*Eric Tonicello & Julien Duboc – ISI Sàrl – Lausanne, Switzerland*

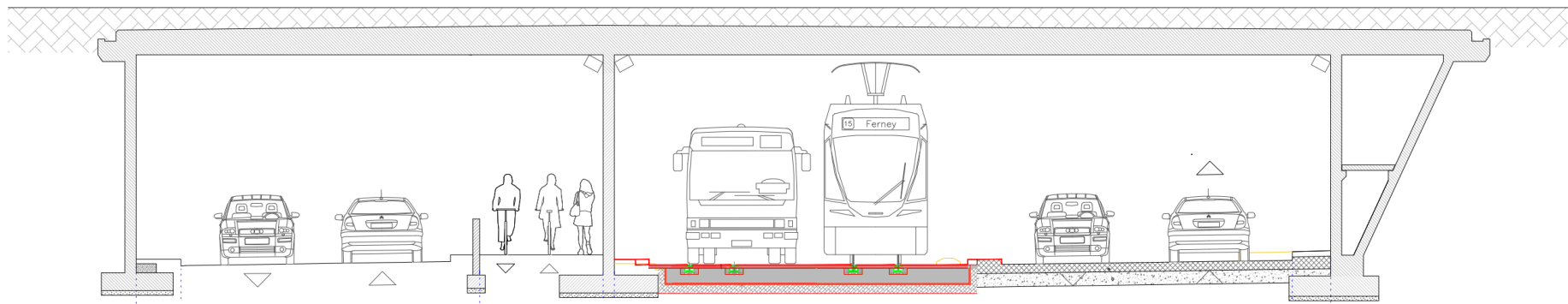




# Description of the project

## Transformation of an existing tunnel

- Road tunnel under the Geneva Airport
- Transformation in the remit of a tramway project
- Check the **fire safety** :
  - ✓ Evacuation
  - ✓ **Structural fire resistance**





# Fire resistance requirements

In Switzerland, no explicit fire duration requirement for tunnel structures

- **Objective:** Get enough time to people escape in safe conditions
  - **R60** as a minimum (sometimes 90 min.)
- **Requirements for this specific tunnel:**
  - Ensure **safe evacuation**
  - **No structural collapse** : Taxiway & Runway
  - No significant deformations

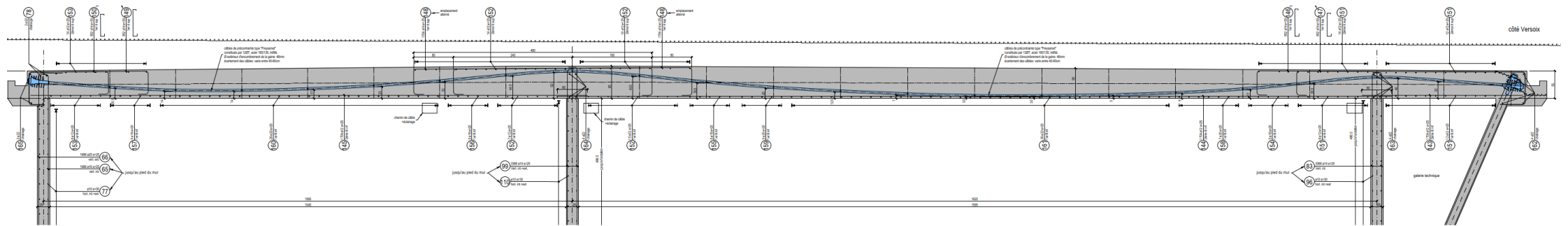




# Structure of the tunnel

## Prestressed concrete structure

- The main structure consists of a double span slab, supported by RC walls
- **~100 %** prestressed-based design on the transversal direction

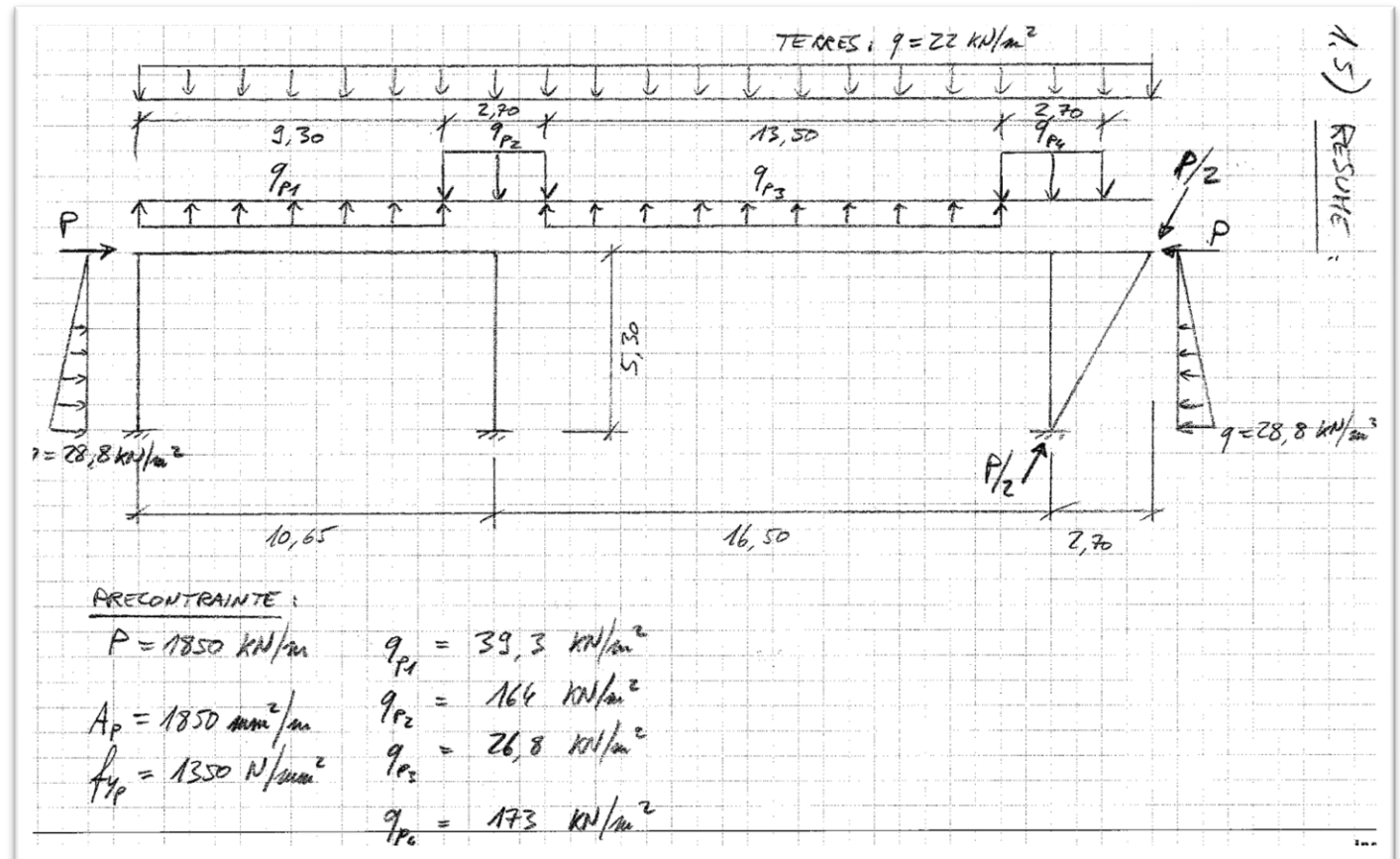




# Structure of the tunnel

## Prestressed concrete structure - design

- Substitute forces to consider prestressed cables
  - $q_{p1}$ ,  $q_{p2}$ ,  $q_{p3}$  and  $q_{p4}$

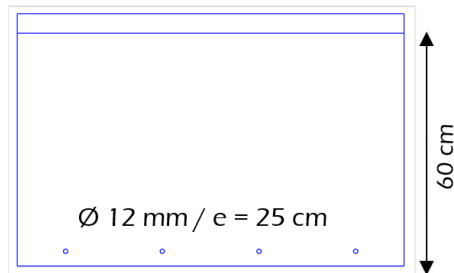
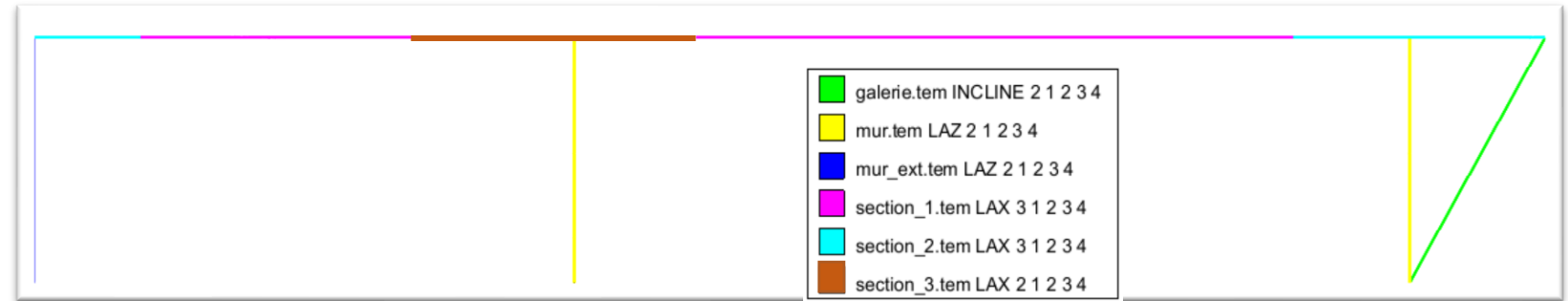




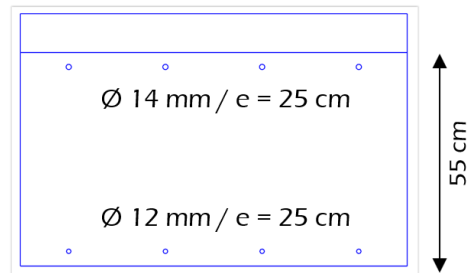
# Structure of the tunnel

## Different sections

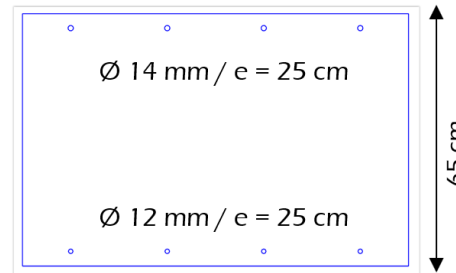
- 3 sections for the slab
- 3 sections for the walls
- «Few» rebars
- Mainly prestressings cables



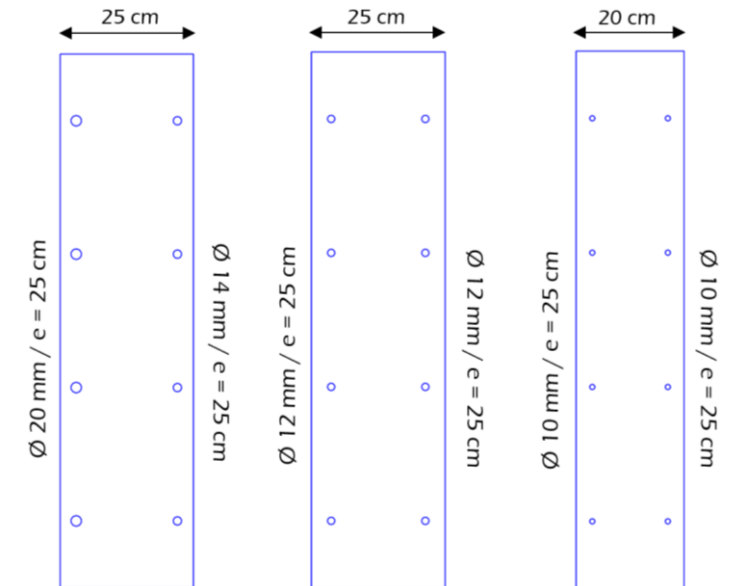
Section\_1



Section\_2



Section\_3



Wall ext

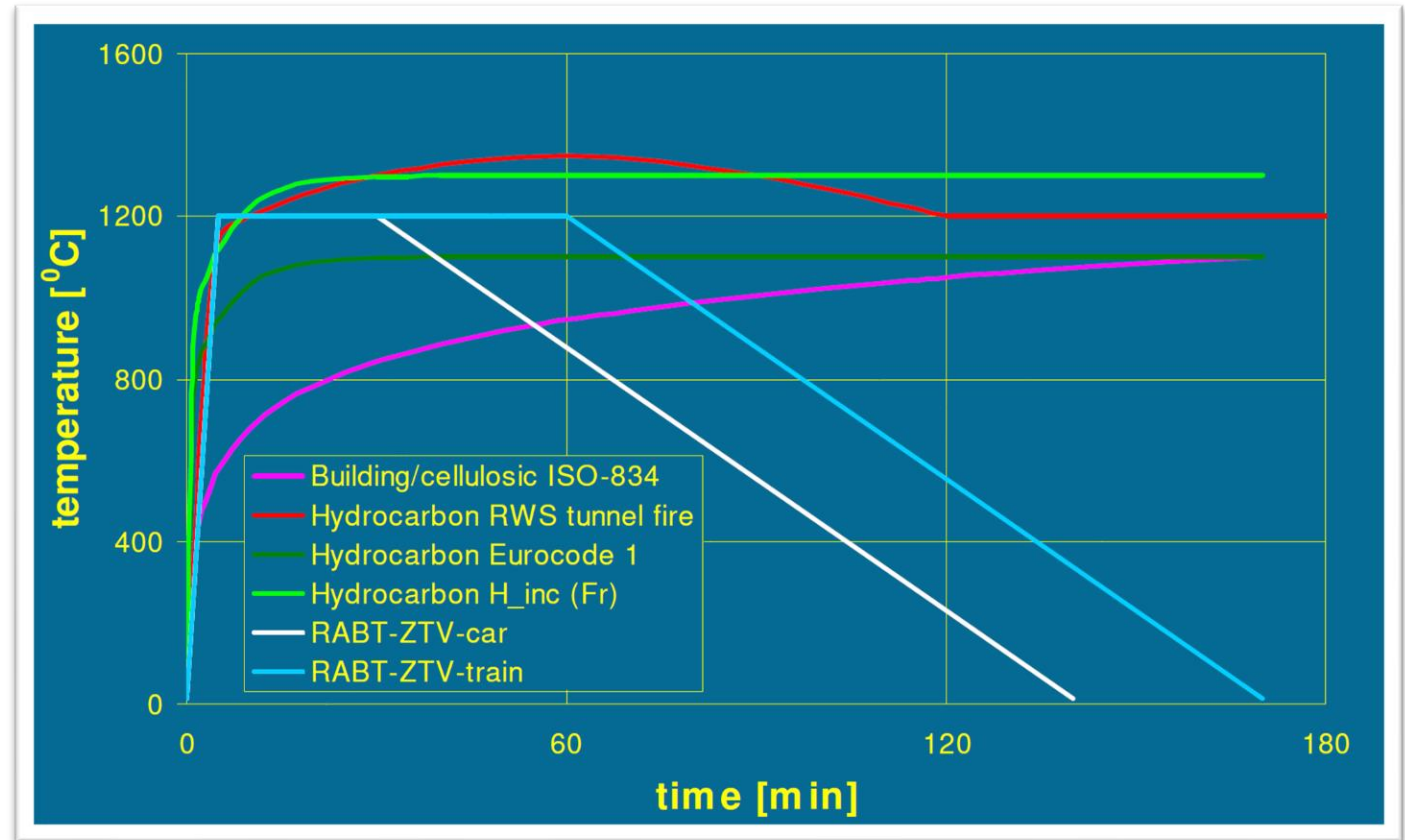
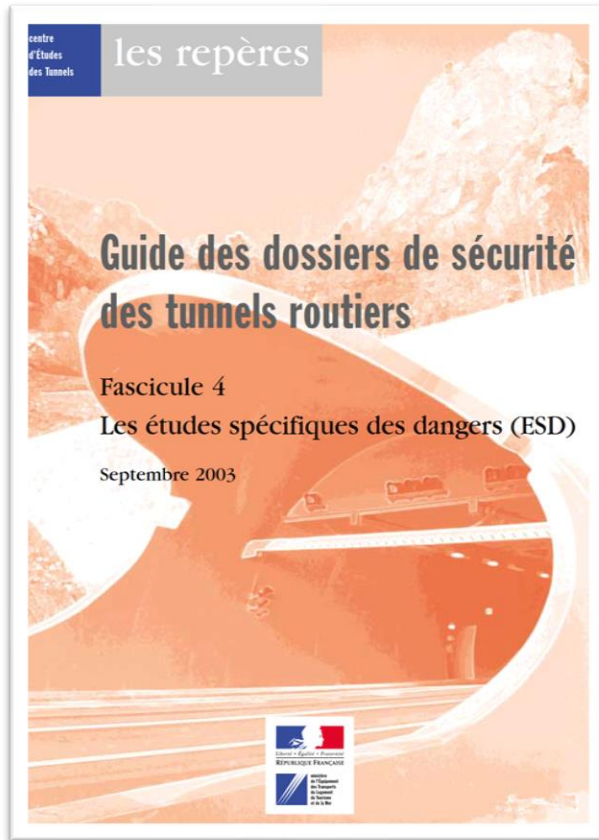
Central wall

Gallery



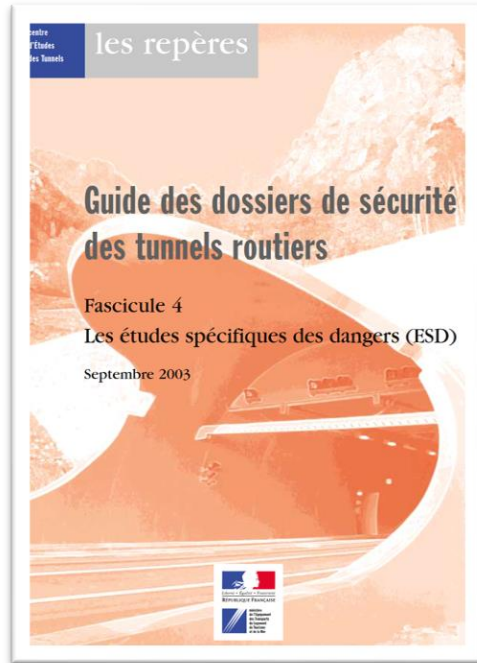
# PBD approach – Step 1 : standard curves

- RWS and ISO fire curves

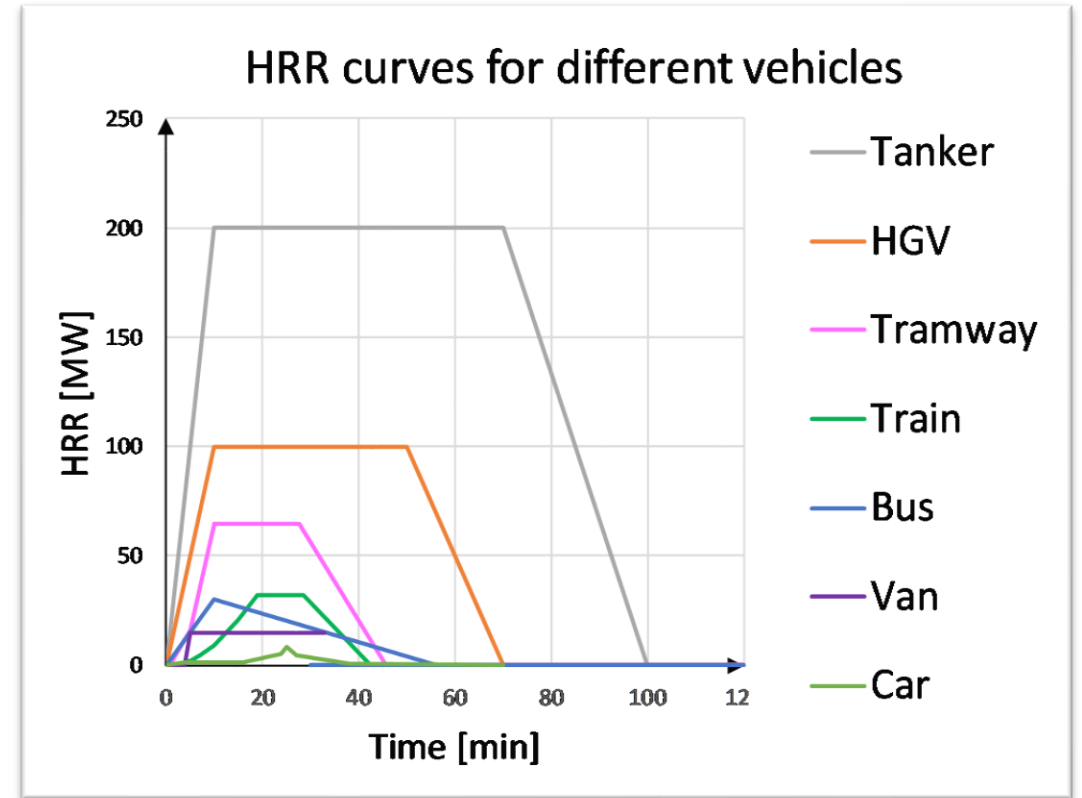




# PBD approach – Step 2: natural fire scenarios



- ✓ Heavy Goods Vehicle fire
- ✓ Fuel tanker fire
- ✓ Tramway fire



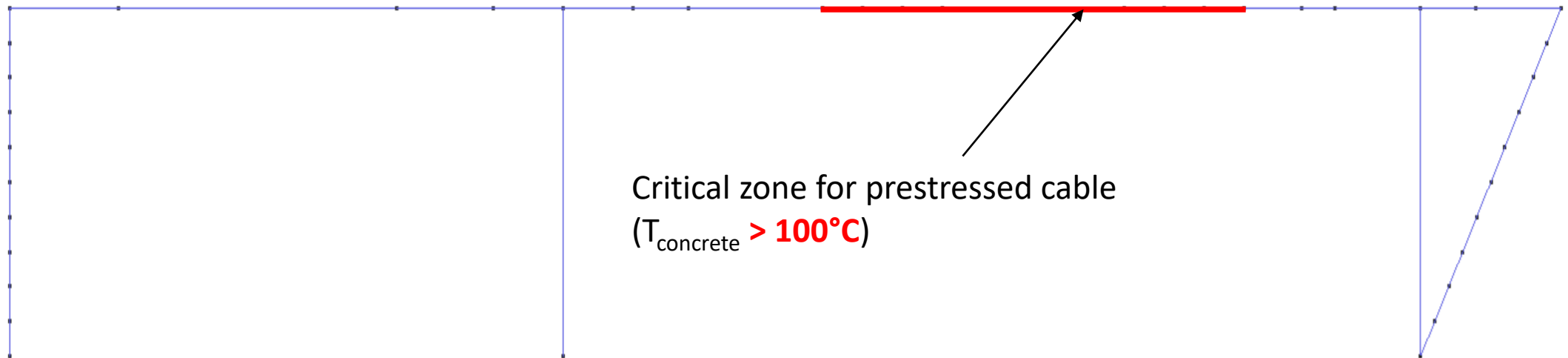




# PBD approach – Standard fire curves

## Thermal calculations

- Check the sensibility of the heating of the prestressing cables

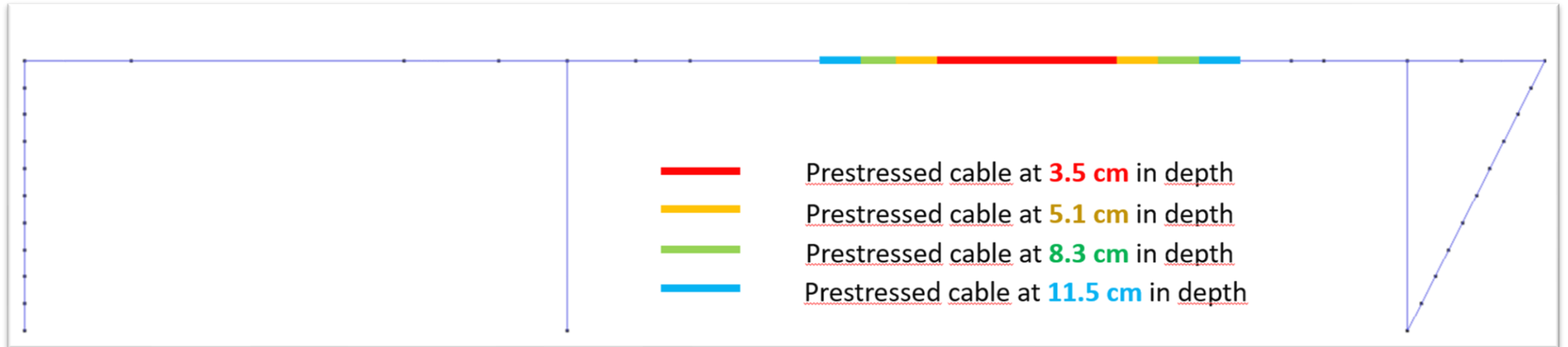




# PBD approach – Checking the prestressing

## Thermal calculations

- Check the sensibility of the heating of the prestressing cables

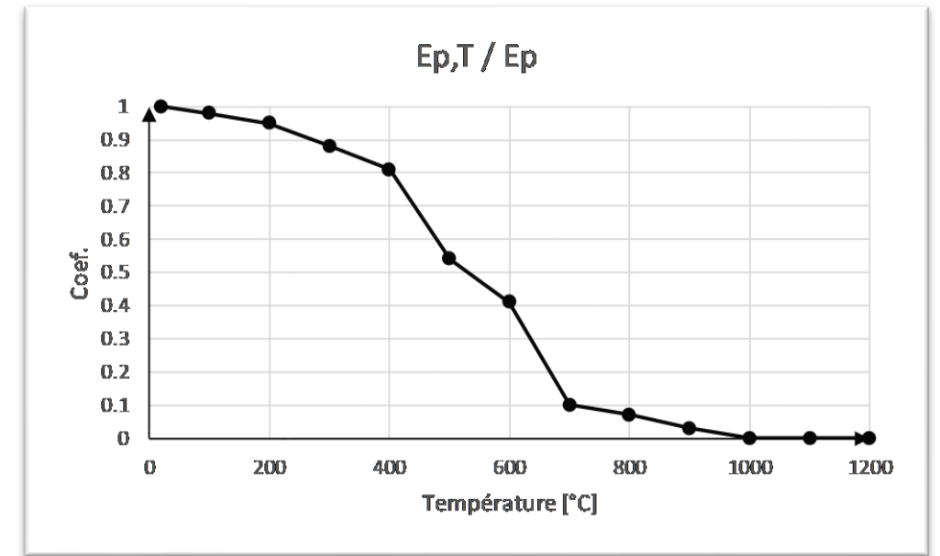
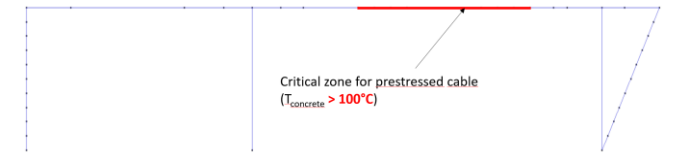
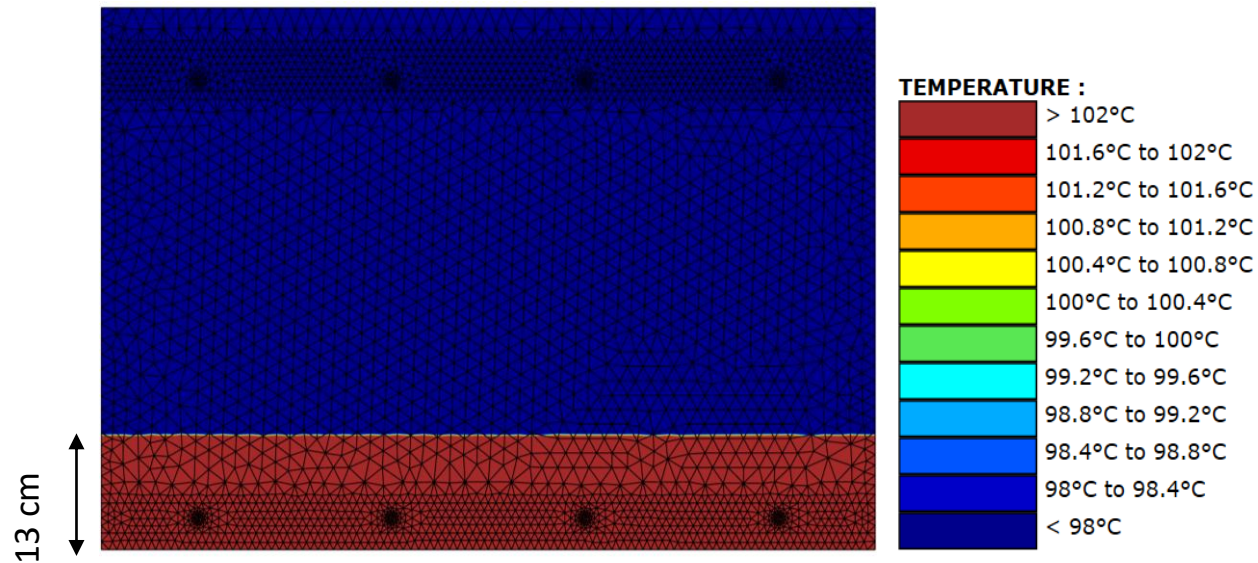




# PBD approach – Standard fire curves

## Thermal calculations

- Temperature evolution in concrete and rebars
- 2D and 3D FEM calculation with SAFIR





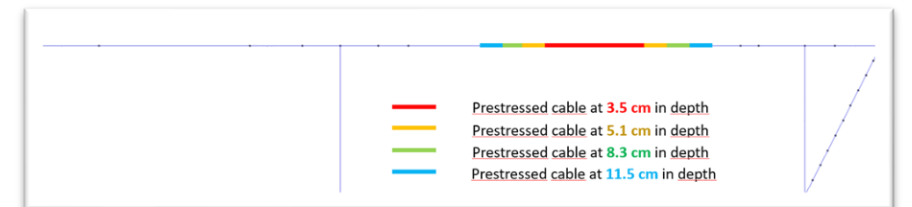
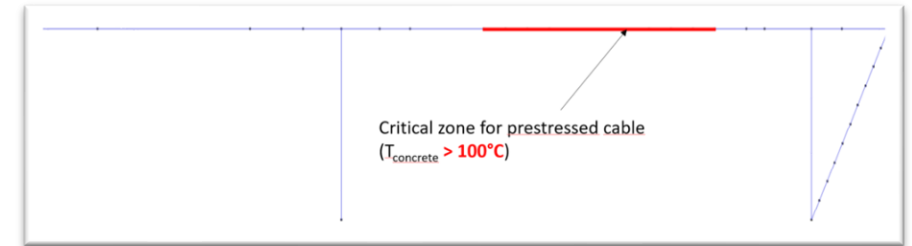
# PBD approach – Standard fire curves

## Thermal calculations

- Temperature evolution in concrete and rebars
- 2D and 3D FEM calculation with SAFIR

## Loss of «substitute forces» due to temperature

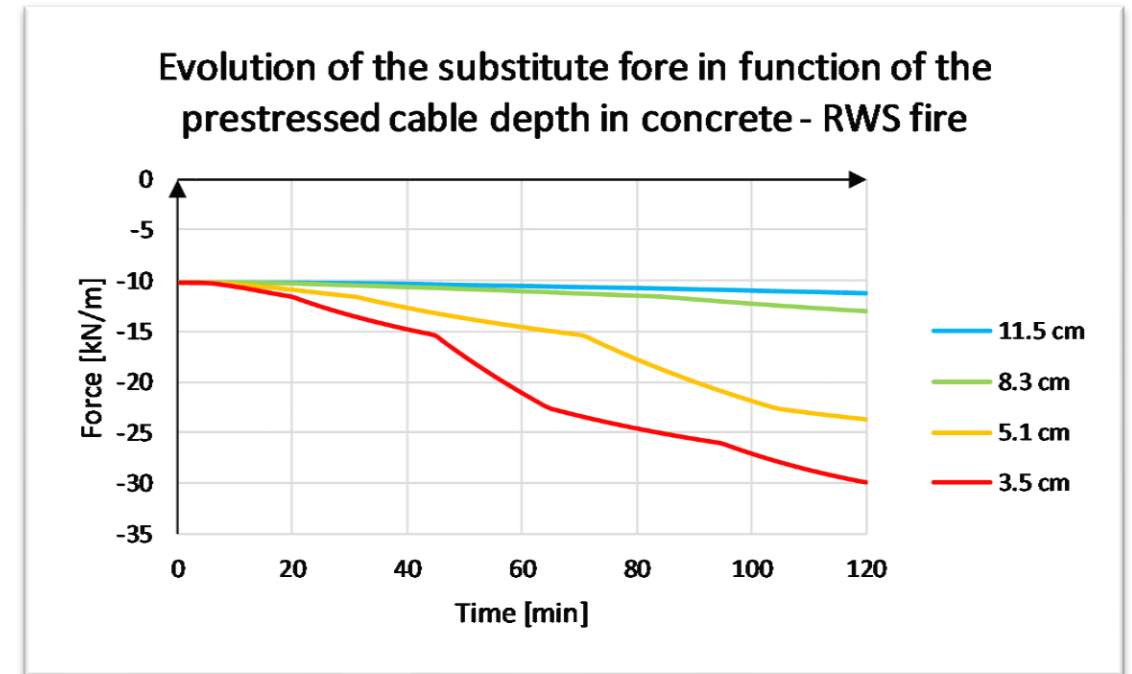
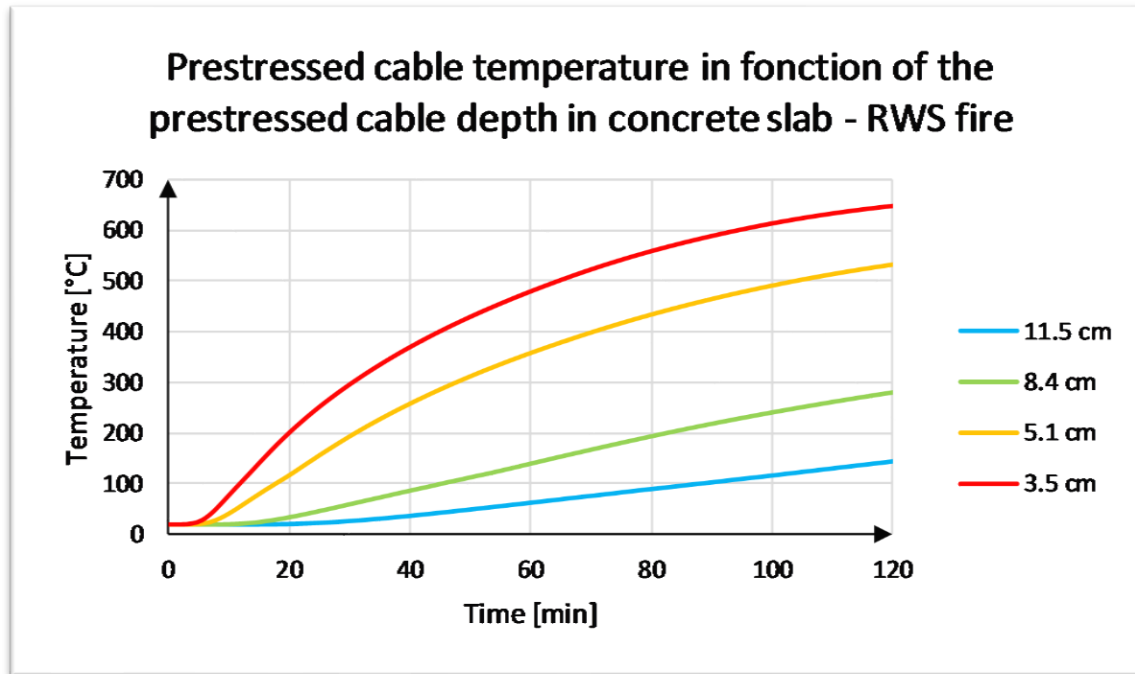
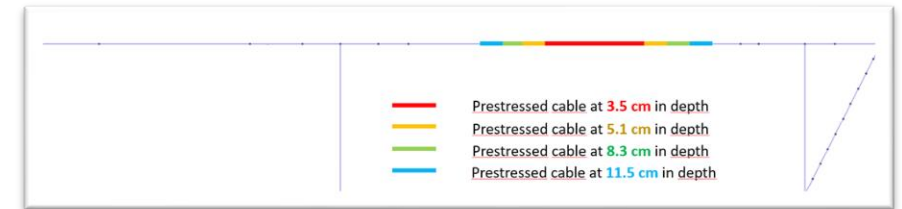
- Thermal elongation
  - ✓  $L_{i+1} = \alpha L_i (T_{i+1} - T_i) + L_i$
- Young modulus reduction
  - ✓ Up to 13 cm in concrete





# PBD approach – Standard fire curves

## Thermal calculations

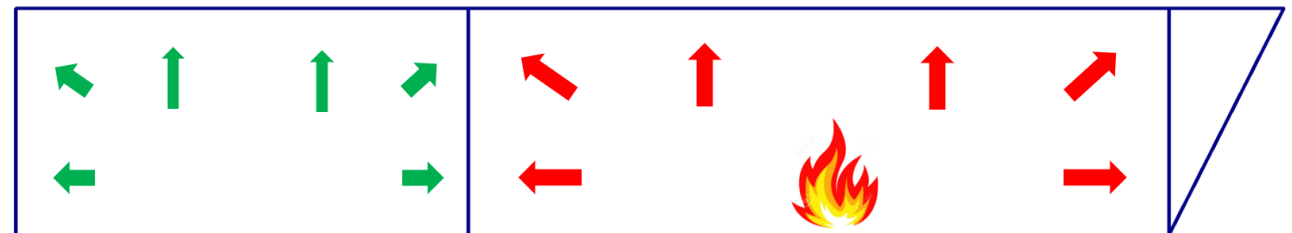
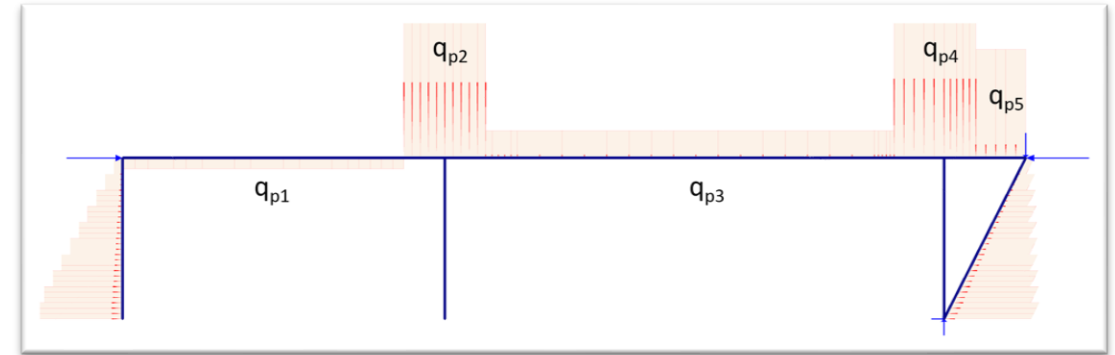




# PBD approach – Standard fire curves

## Structural calculations

- FEM calculation with **SAFIR®**
- Structural model with beam elements
- Loading conditions in function of temperature
  - According to thermal calculations
- Fire scenario in the right section :

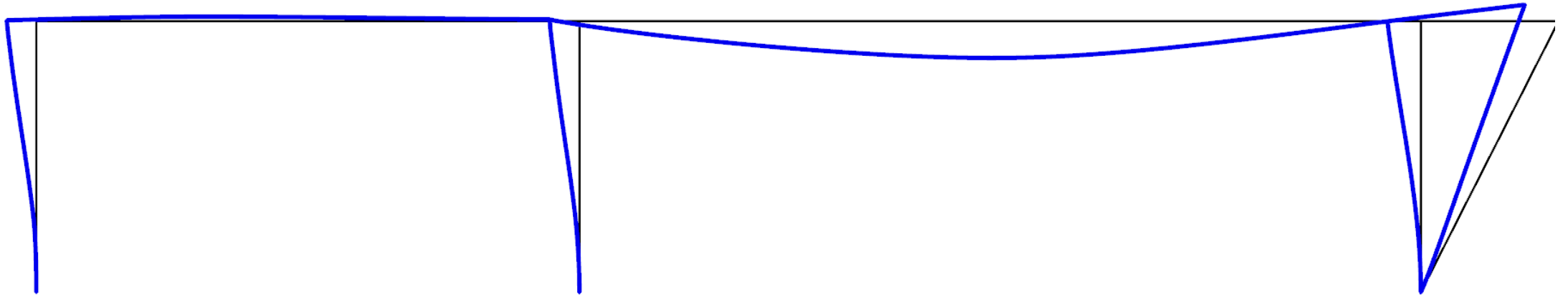




# PBD approach – Standard fire curves

## Structural calculations

- FEM calculation with SAFIR



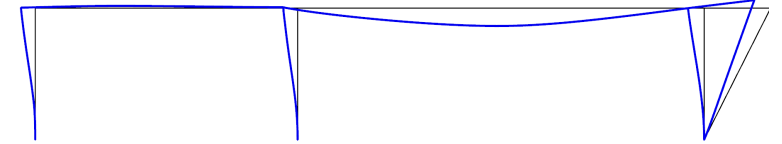
*Structural FEM model: initial state (black) / deformed state (blue)*



# PBD approach – Standard fire curves

## Structural calculations

- FEM calculation with SAFIR
- Pre-stress concrete structure < R60
- High deformations → collapse
  - Structure should be replaced
  - Significant interruption of Airport activities



| Structural resistance of tunnel in fire situation | PBD results               |                           |                            |
|---|---------------------------|---------------------------|----------------------------|
|   | Fire resistance [minutes] | Maximum deformations [mm] | Residual deformations [mm] |
| ISO fire  | 36                        | Collapse                  |                            |
| RWS fire  | 27                        | Collapse                  |                            |







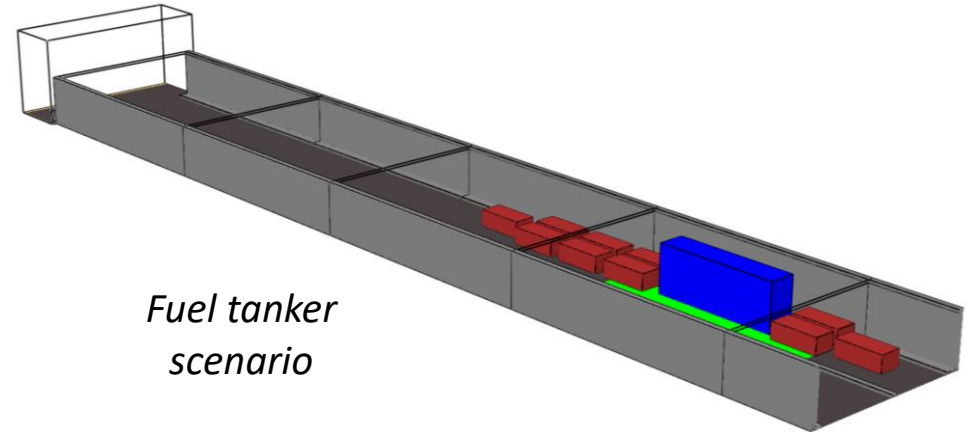
# PBD approach – Natural fire scenarios

## CFD calculations with FDS

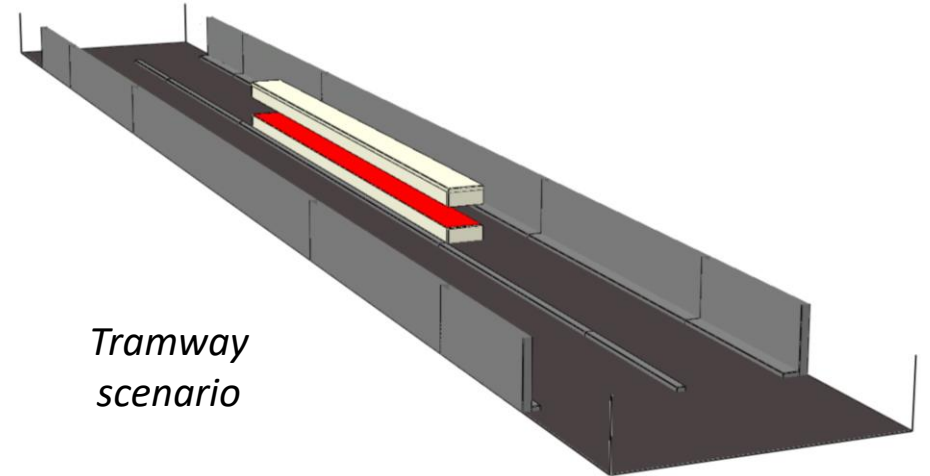
- Geometry of the tunnel
- Reaction of combustion
- Natural ventilation

## HRR curves according to CETU guide

- Fuel tanker 200 MW
- HGV 100 MW
- Tramway ~64 MW (publications)



*Fuel tanker scenario*



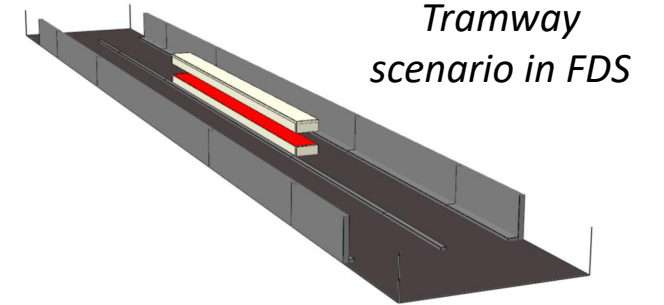
*Tramway scenario*



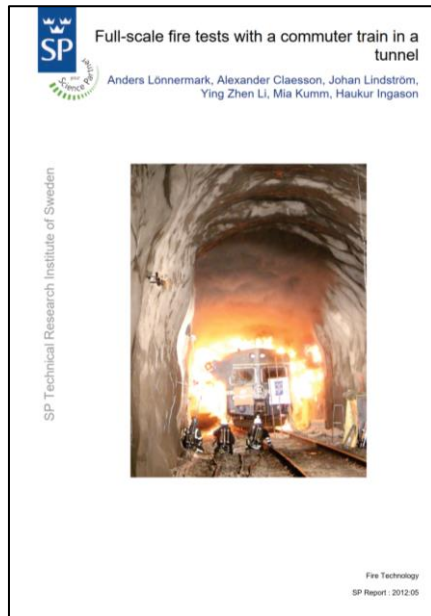
# PBD approach – Natural fire scenarios

## Tramway 64 MW

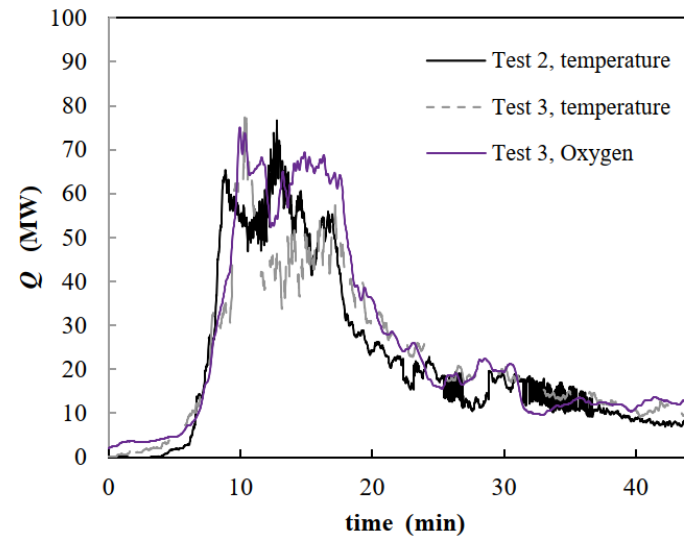
- HRR curve according to publications and experiments for train fires



Tramway scenario in FDS



Publication as reference



HRR tests in experiments



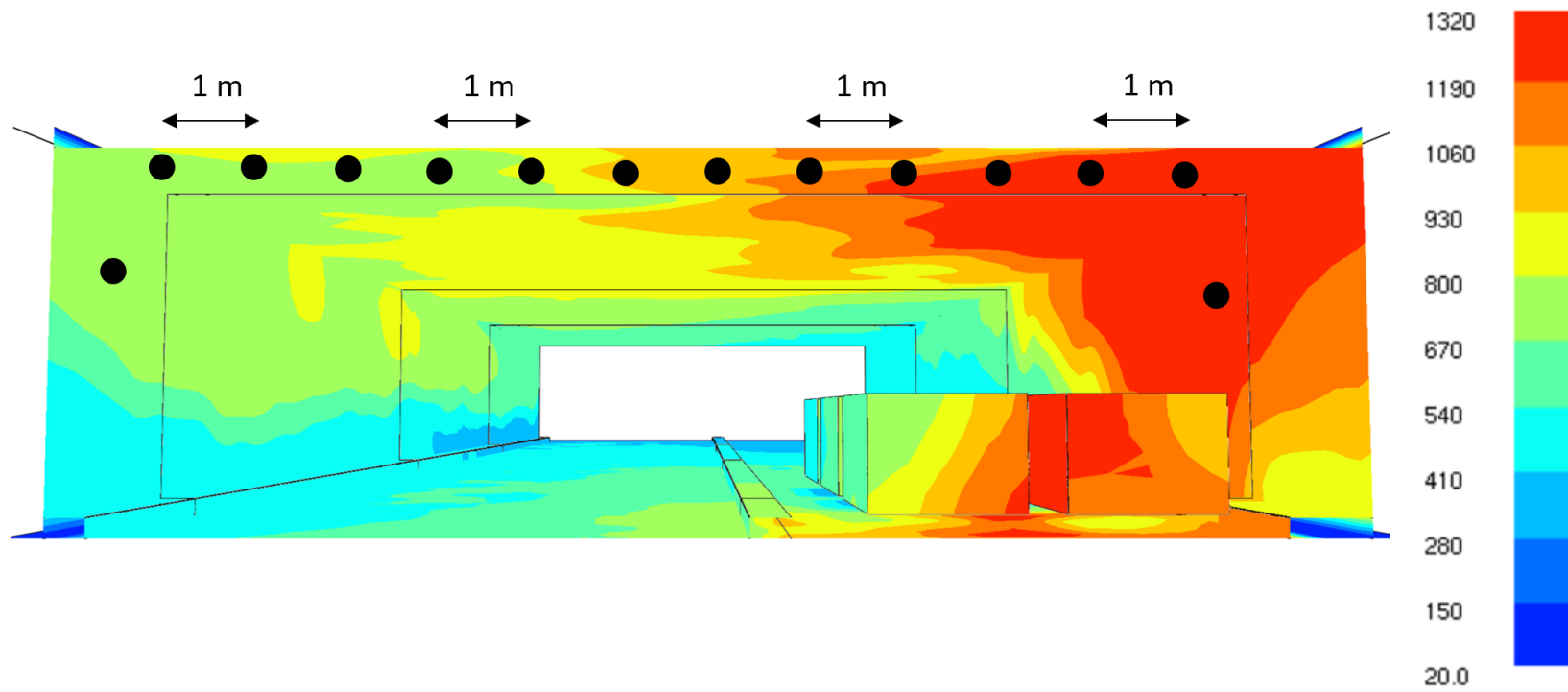
Additional fire load density considered



# PBD approach – Natural fire scenarios

## CFD calculations with FDS

- AST devices on ceiling and walls

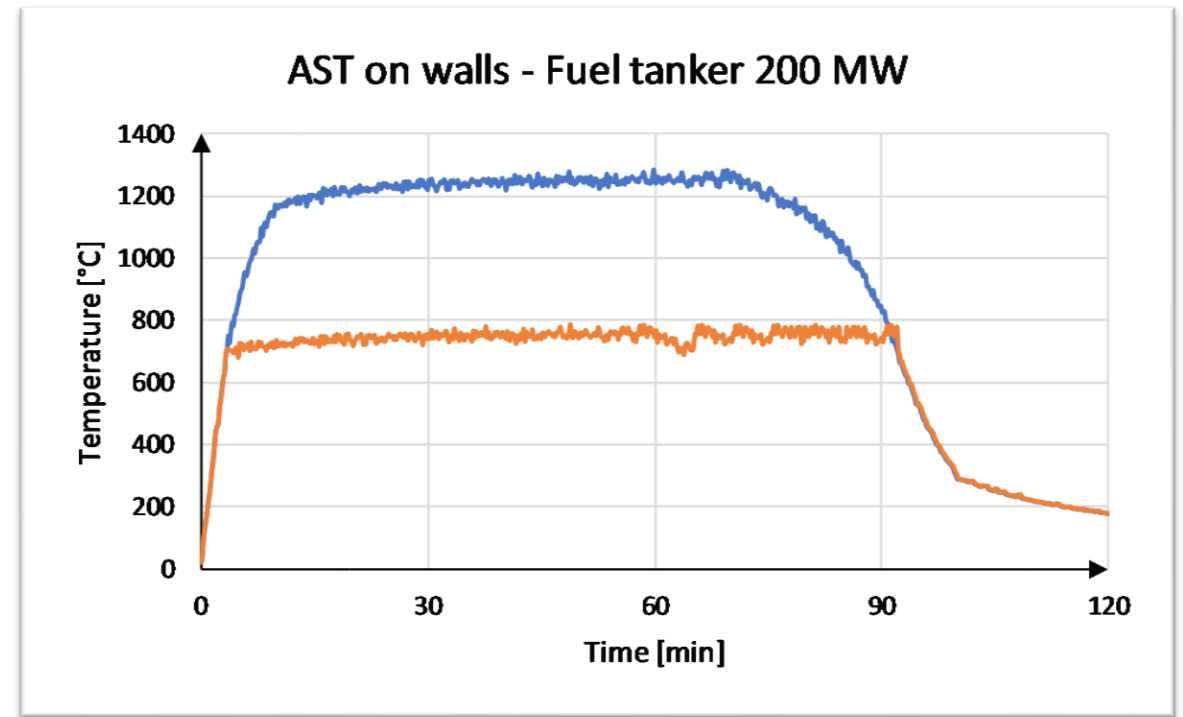
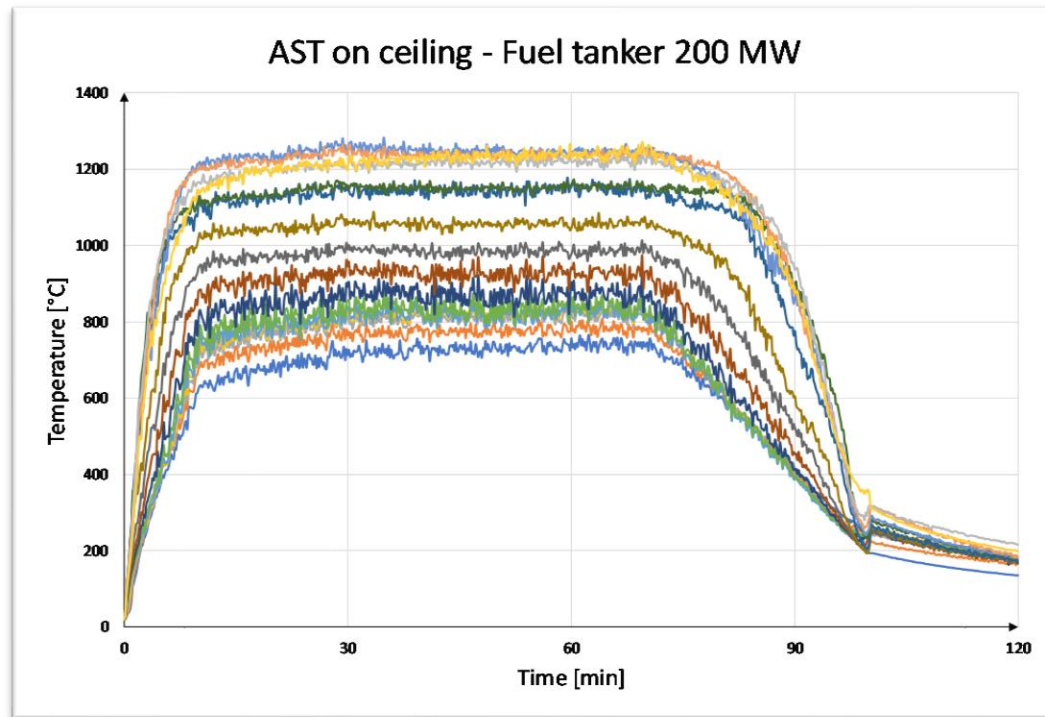
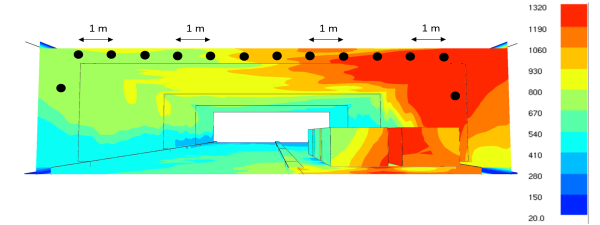




# PBD approach – Natural fire scenarios

## CFD calculations with FDS

- AST devices on ceiling and walls

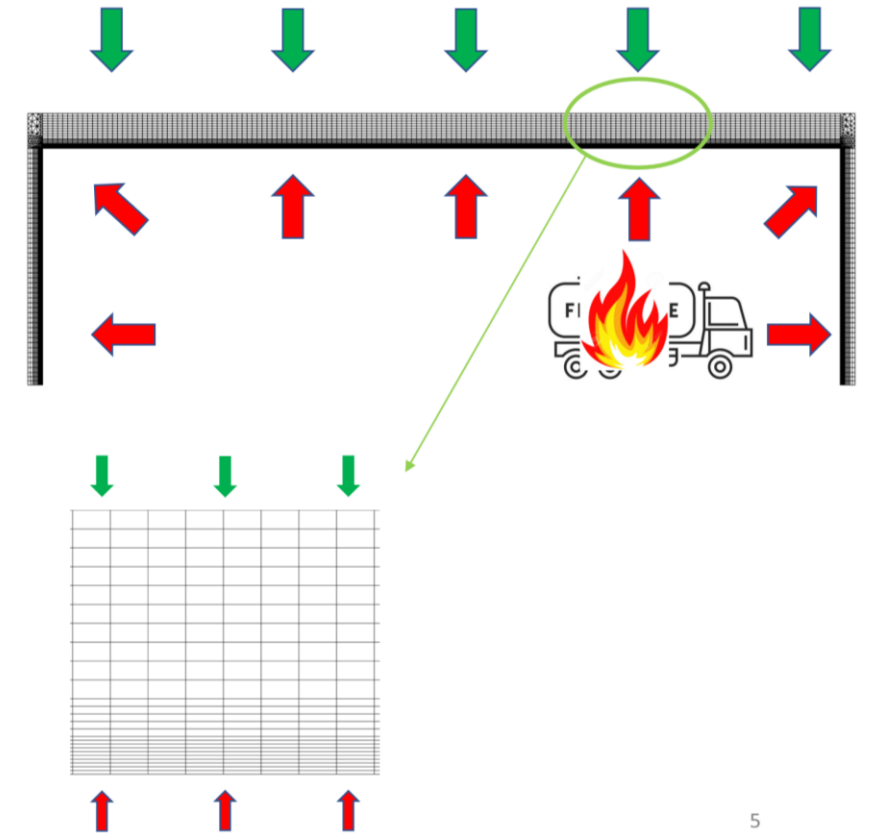
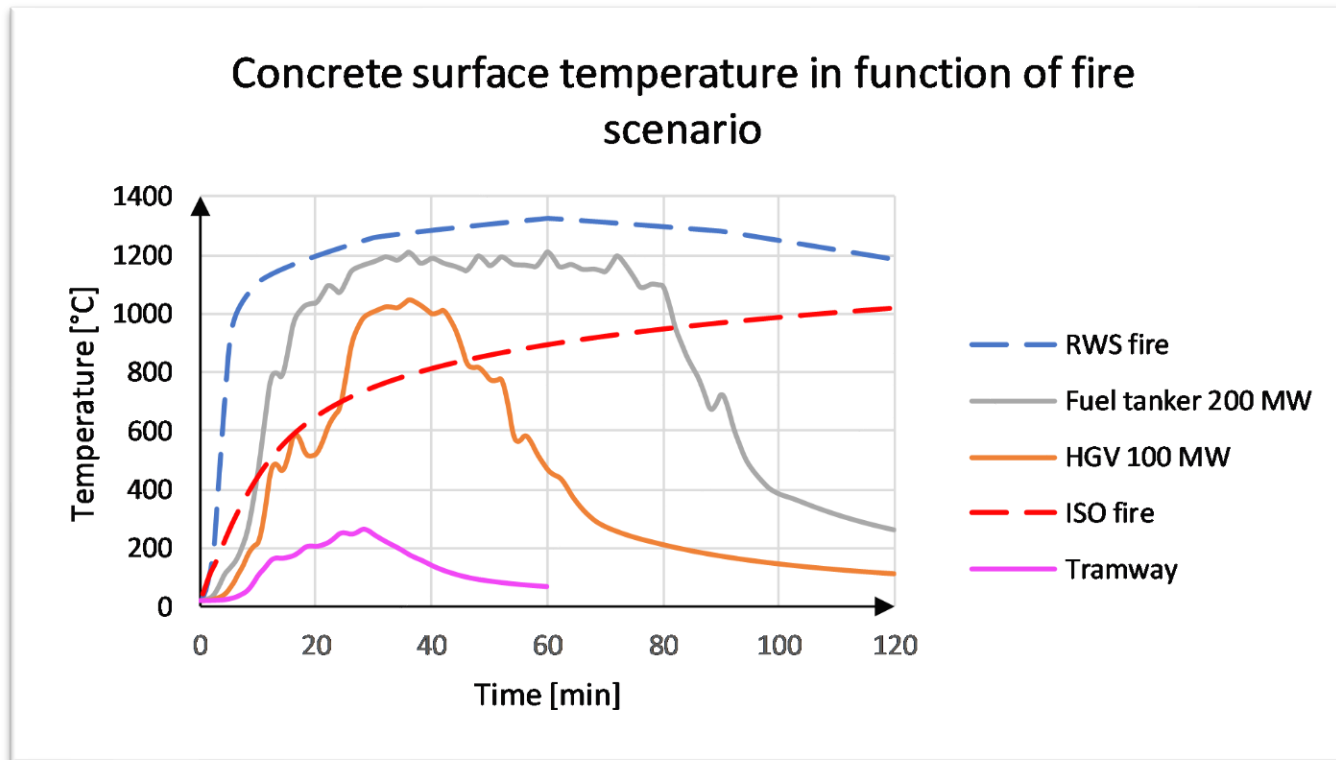




# PBD approach – Natural fire scenarios

## Thermal calculations

- Thermal stresses of CFD model as boundary conditions



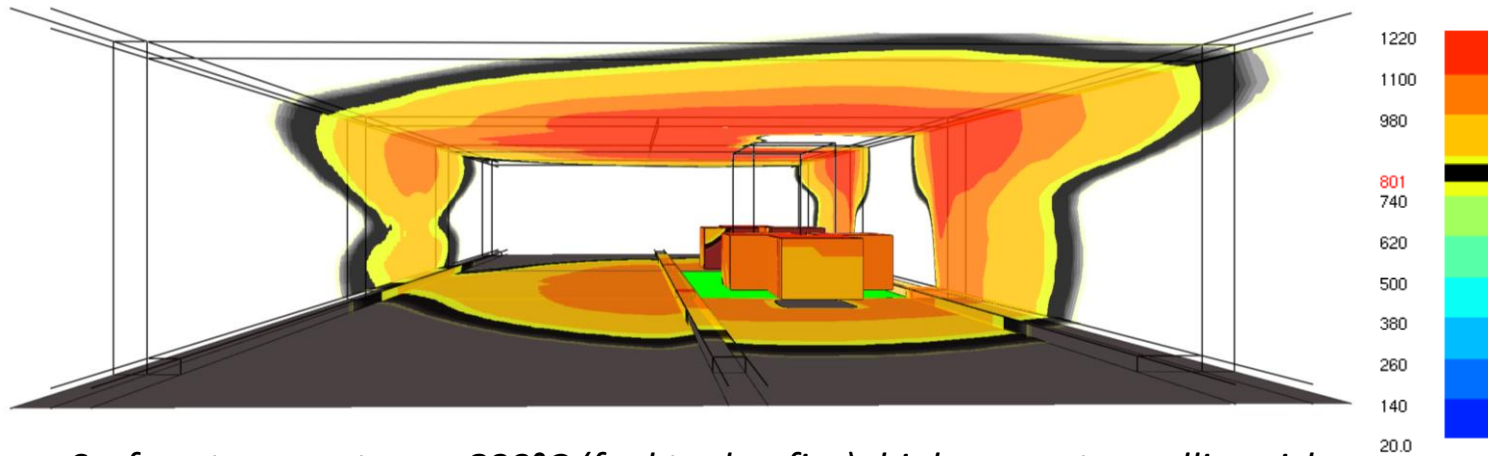


# PBD approach – Natural fire scenarios

## Structural calculations

- ISO / RWS / 100 MW / 200 MW: **KO**
- Tramway: **OK**
- No spalling considered
  - ~600 – 800°C

| Structural resistance of tunnel in fire situation | PBD results               |                           |                            |
|---|---------------------------|---------------------------|----------------------------|
|   | Fire resistance [minutes] | Maximum deformations [mm] | Residual deformations [mm] |
| ISO fire  | 36                        | <b>Collapse</b>           |                            |
| RWS fire  | 27                        | <b>Collapse</b>           |                            |
| Tramway   | <b>OK</b>                 | 25                        | 13 - 15                    |
| HGV 100 MW  | 28                        | <b>Collapse</b>           |                            |
| Fuel tanker 200 MW                                | 27                        | <b>Collapse</b>           |                            |



Surface temperature > 800°C (fuel tanker fire): high concrete spalling risk



Concrete spalling example

# PBD approach – Natural fire scenarios

## Solutions:

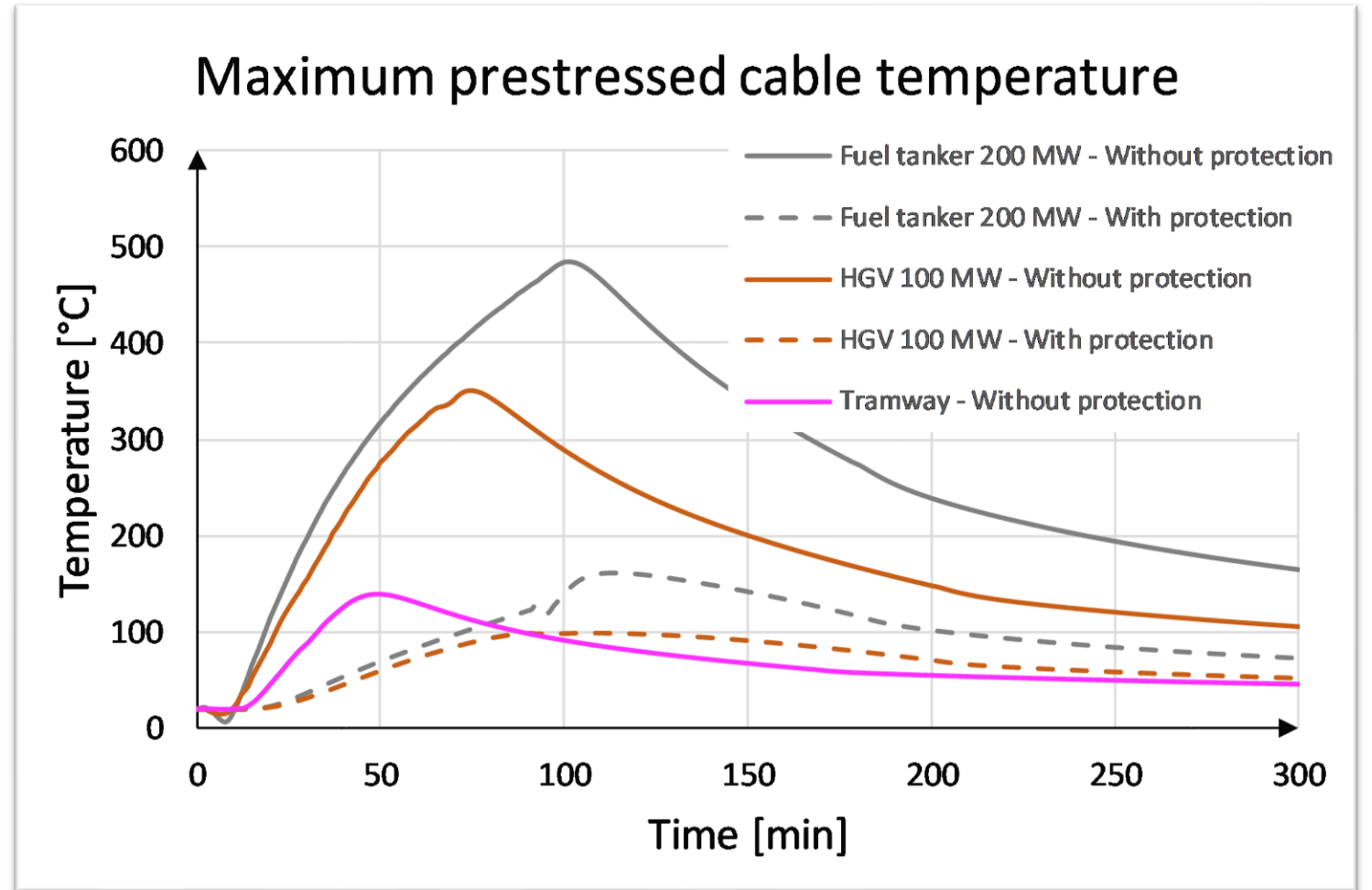
- **Organisational measures** → no HGV and non fuel tanker in this tunnel (*must take another itinerary*)
- **Passive measures** → Fire panels (*Promatect-H EI90 or similar*)
- **Active measures** → **Water mist installation**

| Structural resistance of tunnel in fire situation | PBD results               |                           |                            |
|---|---------------------------|---------------------------|----------------------------|
|   | Fire resistance [minutes] | Maximum deformations [mm] | Residual deformations [mm] |
| ISO fire  | 36                        | Collapse                  |                            |
| RWS fire  | 27                        | Collapse                  |                            |
| Tramway   | OK                        | 25                        | 13 - 15                    |
| HGV 100 MW  | 28                        | Collapse                  |                            |
| Fuel tanker 200 MW                                | 27                        | Collapse                  |                            |

# SG PBD approach – Solutions

## Passive measures

- Walls and main part of the slab **need to be protected**

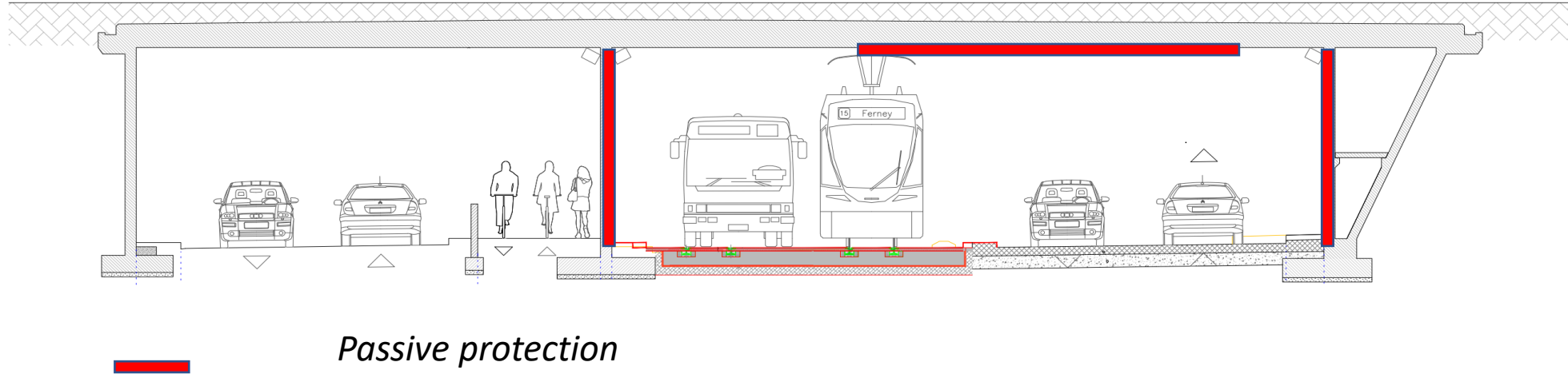
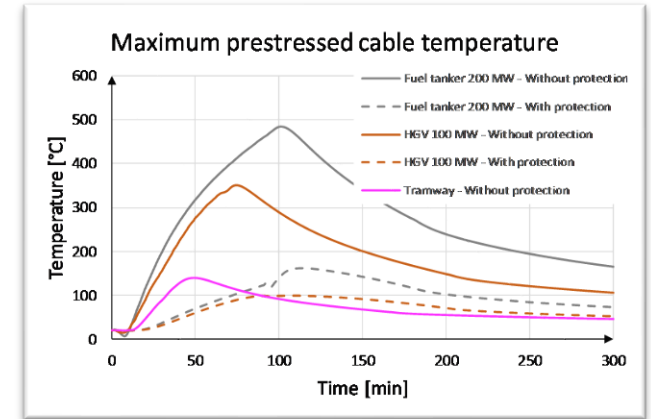




# ■ PBD approach – Solutions

## Passive measures

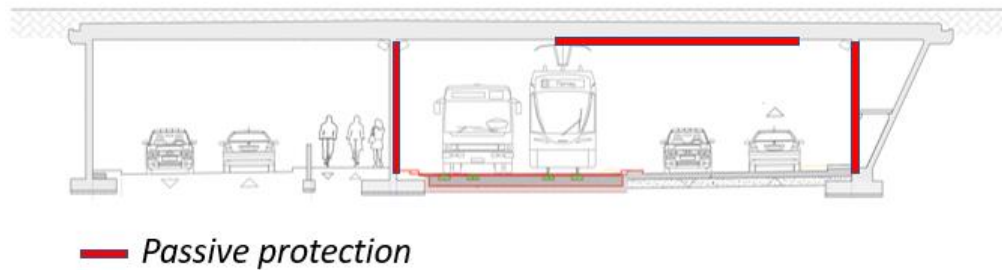
- Walls and main part of the slab need to be protected



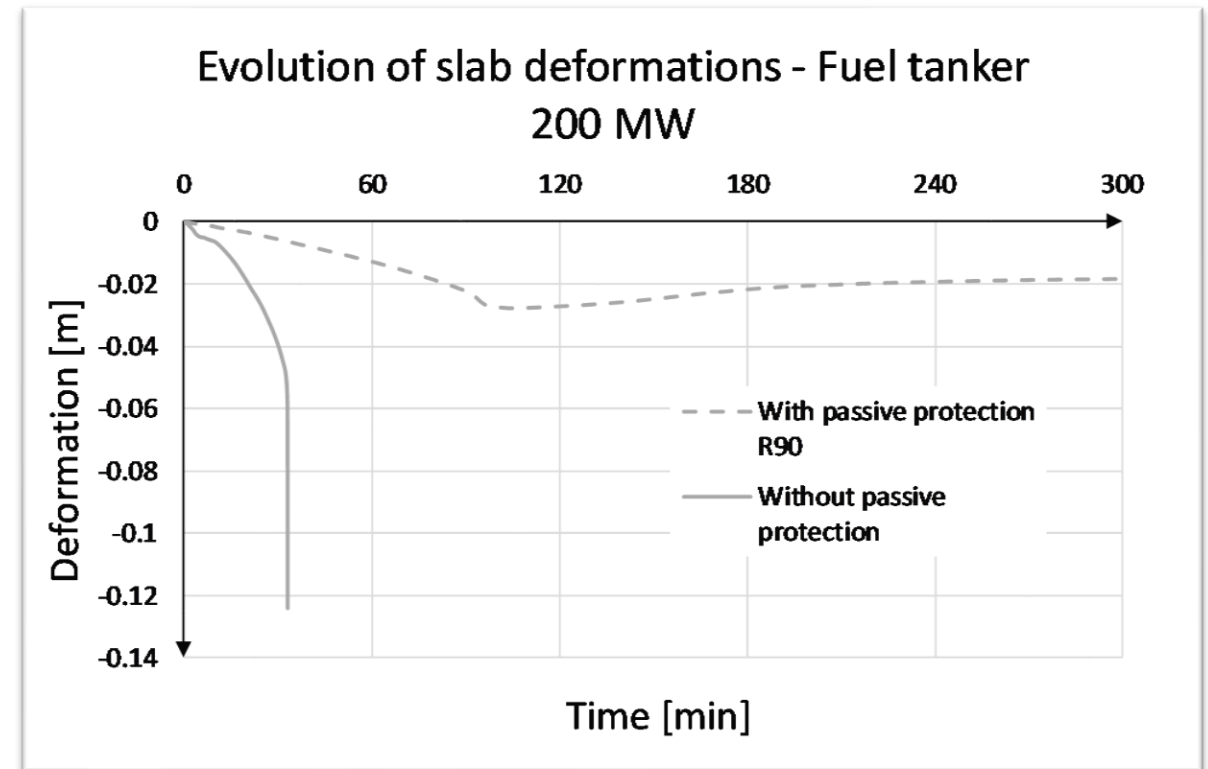
# PBD approach – Solutions

## Passive measures

- Walls and main part of the slab need to be protected



- Low deformations with **EI90 protection**
  - Promatect-H 25 mm or similar*

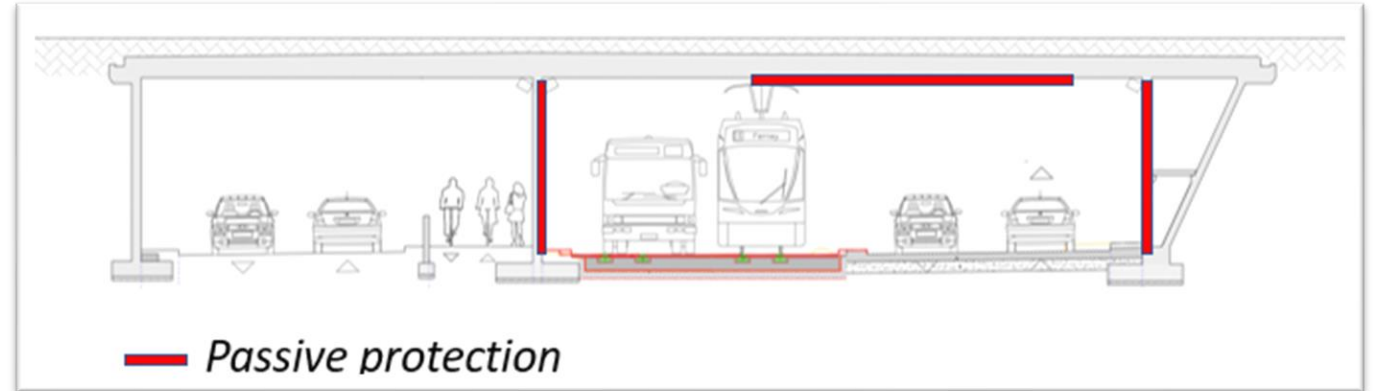


# PBD approach – Solutions

## Passive measures

### ■ Advantages:

- System reliability
- Less maintenance
- Very efficient
- Good feedback



### ■ Drawbacks:

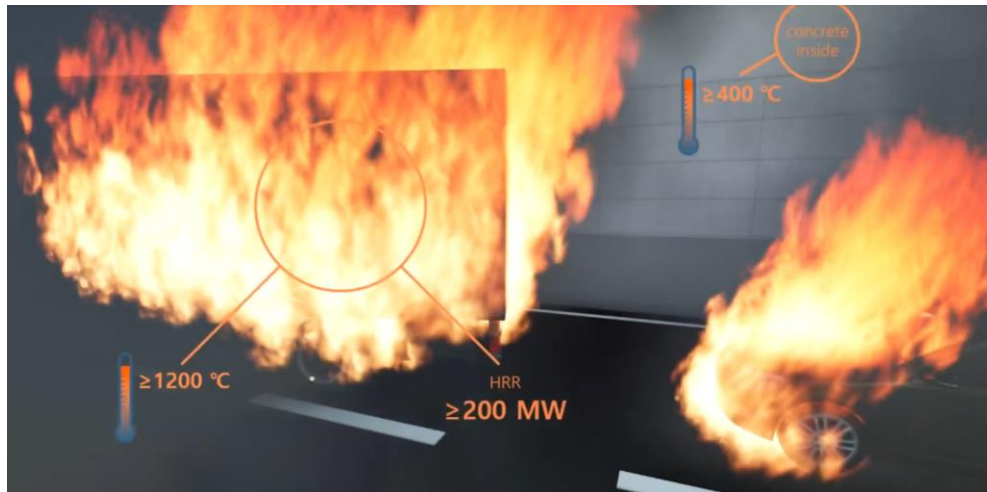
- **Very expensive solution ~450 € / m<sup>2</sup>**
- (brand new) Technical installations to be replaced *post-fire*
- Fire panels have to be replaced post-fire (need to close tunnel)
- No (cooling) effect on fire



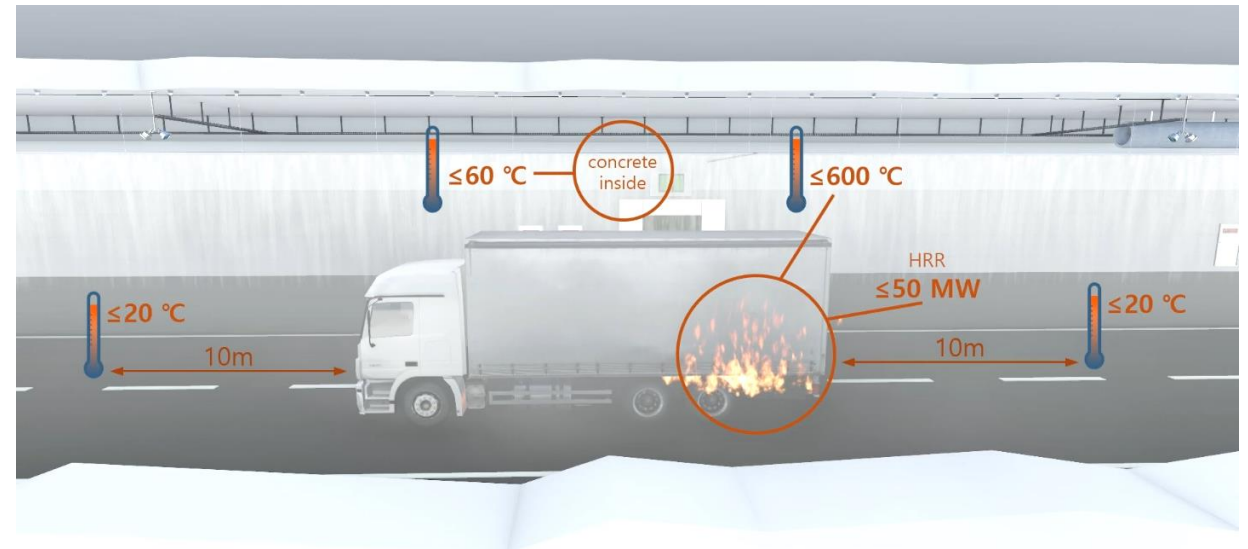
# SG PBD approach – Solutions

## Active measure: water mist solution

- Tested up to 250 MW fire



*Without water mist system*



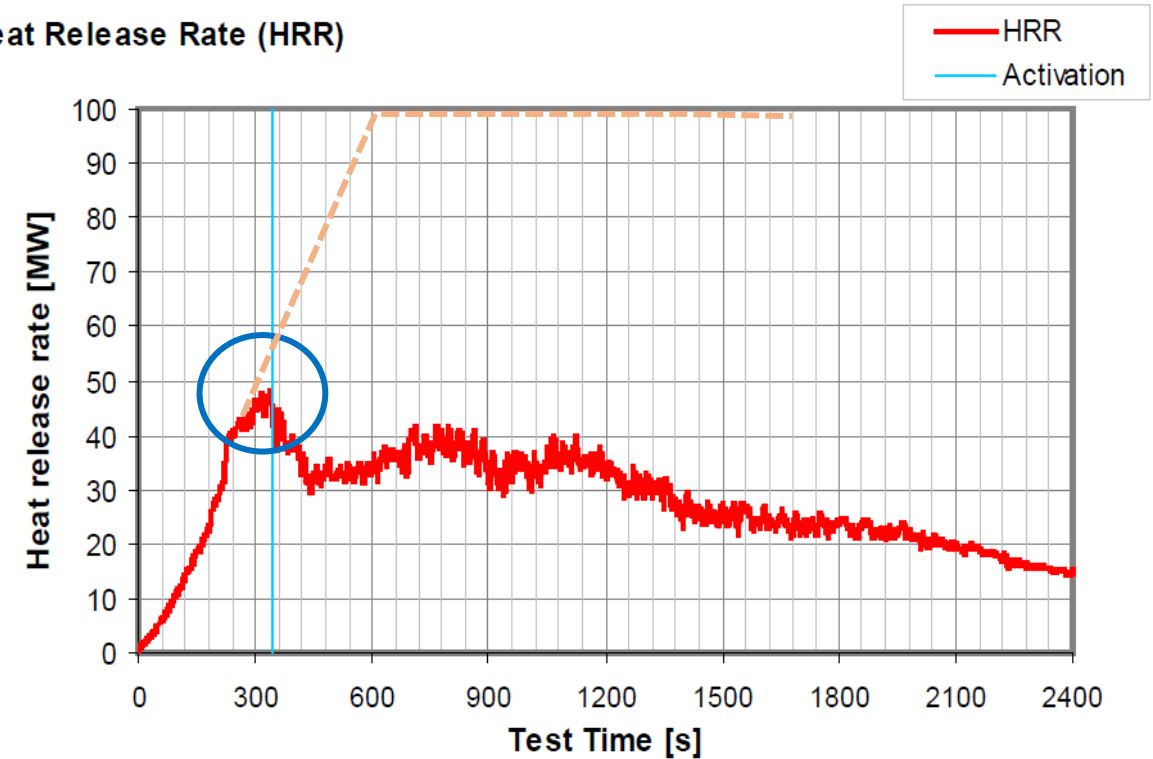
*With water mist system*

# PBD approach – Solutions

## Active measure: **water mist solution**

- Tested up to 250 MW fire
- **Cooling effect** on fire after activation
- Quick HRR mitigation at the activation time

Heat Release Rate (HRR)



*Test for HGV fire – 100 MW*

# PBD approach – Solutions

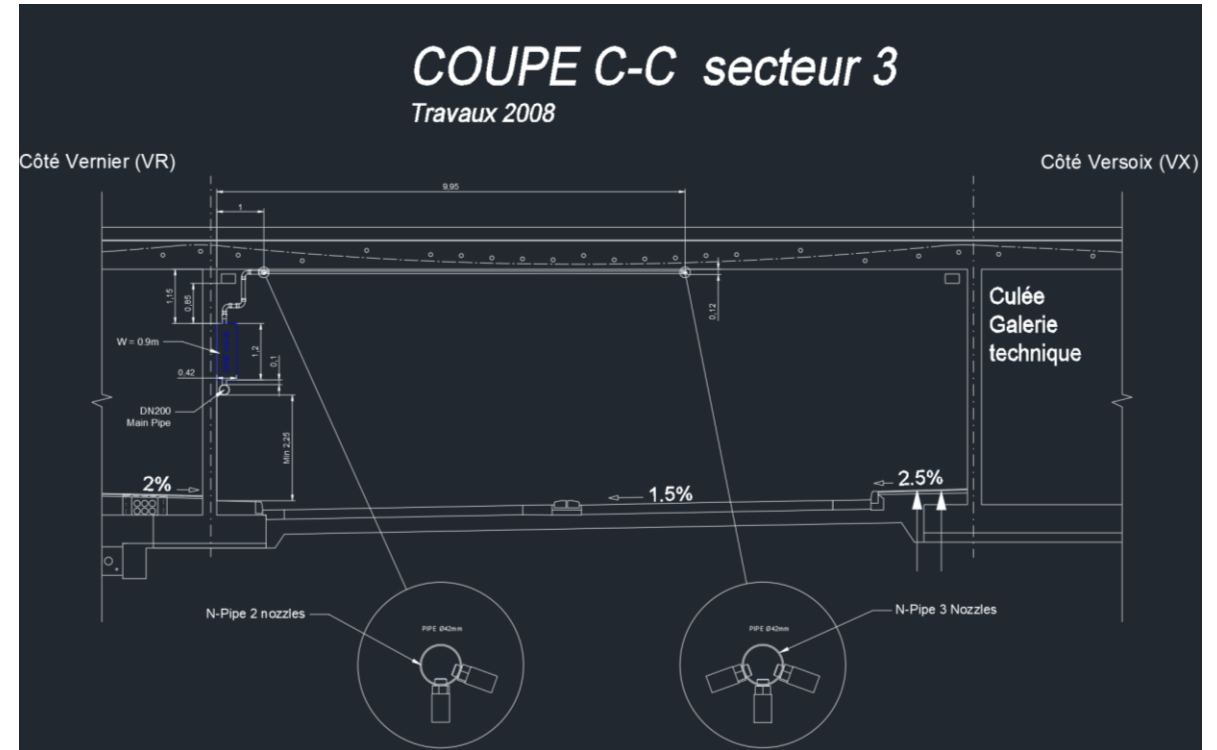
## Active measure

### ■ Advantages:

- Limited fire development
- Easier and safer for the firefighting
- Low damage risk for tunnel structures and technical installations

### ■ Drawbacks:

- Reliability  $90 < P < 98 \%$
- Damages to nozzles (clogging, impacts)
- Smoke destratification (evacuation)
- Maintenance required





# Results and conclusion

Current **structural situation** is unacceptable in case of fire

- Huge deformations of the slab → **collapse very likely to happen**
- Incompatibility with Airport activities (can't be closed or interrupted for days)

Need to **improve structural behavior and safety**

- Mixed solution: localized passive protection + active measure
  1. **Fire panels in the most sensitive parts of the structure**
  2. **Full water mist system coupled to a smoke/thermal/camera detection**

PBD approach offers best solutions to clients in order to **improve safety of structures and guaranty the airport operations**



Thanks for you attention

Questions are welcome 😊

Eric Tonicello – ISI Sàrl – Lausanne, Switzerland – [eric.tonicello@incendie.ch](mailto:eric.tonicello@incendie.ch)

Julien Duboc – ISI Sàrl – Lausanne, Switzerland – [julien.duboc@incendie.ch](mailto:julien.duboc@incendie.ch)